

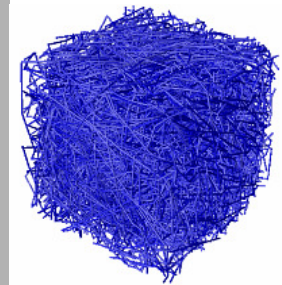
Simulation Based Optimization of Layered Non-wovens as Acoustic Trims

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Overview

Background and motivation

Virtual acoustic material design in a nutshell

Non-wovens as absorbers – effective material models

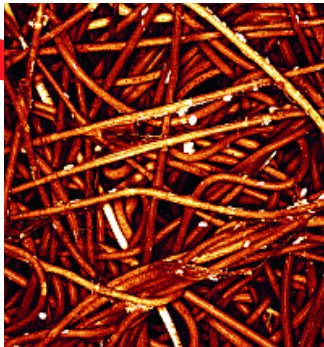
Layered structures

Compression simulation

Acoustic properties of compressed non-wovens

Summary and outlook

Physical and mathematical formulation of multiscale problems



Material: Parts:

Nano- and micrometers

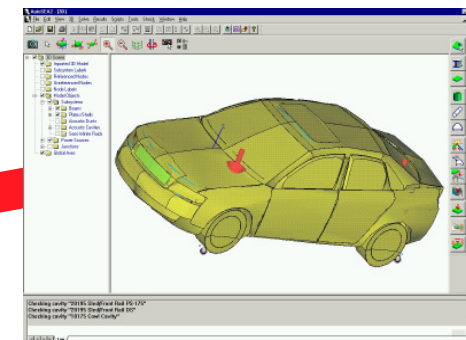
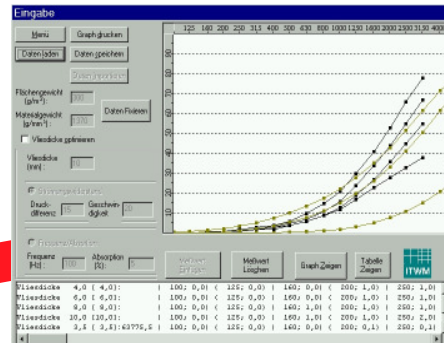
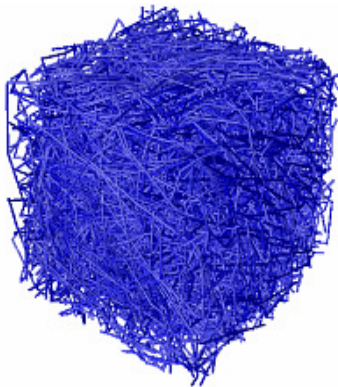


System:

Centimeter



Meter



Virtual material design versus an empirical process

Empirical process

Material production and testing

(acoustic measurement in impedance tube or alpha cabin)

Disadvantages:

- Prototyping is time consuming and expensive!
- Measurements are demanding
- Instead of an optimisation only small improvements are possible

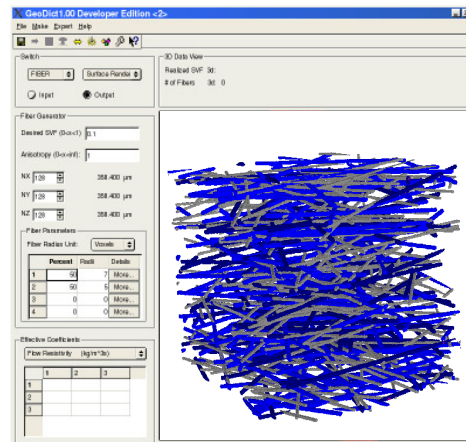
Virtual material design

- The microstructure (e.g. Non-woven) is generated entirely on the computer
- Determination of effective material parameters by numerical simulation

Advantages:

- No prototyping required
- Extensive parameter studies can be done with moderate efforts
- Potential for computer aided optimisation

ITWM-Softwaretool GeoDict (*Geometry* generation and *prediction*)

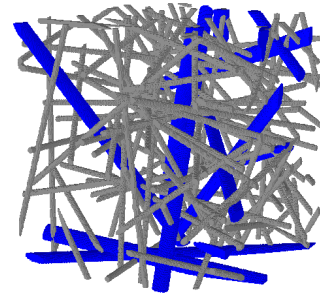


Interactive
microstructure
generator

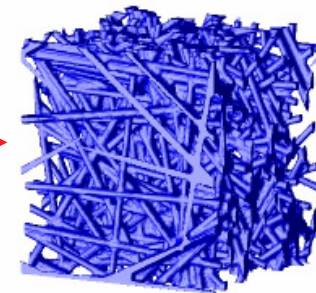
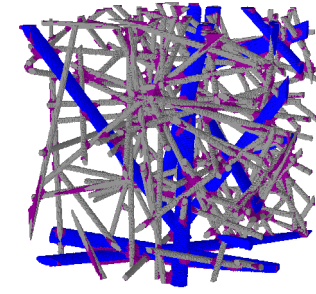
www.geodict.com



80% PET fibers, 7dtex
20% PP fibers, 2.2 dtex
Area weight: 200 g/m²

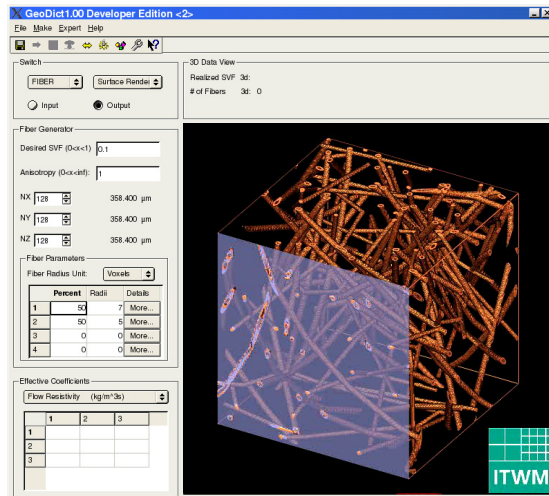


50% PET fibers, 60dtex, elliptic cross section
50% PP fibers, 8 dtex, circular cross section
95% porosity, with and without binder



Carbon paper,
used as gas
diffusion layer in
a fuel cell
70% porosity

Parameter prediction: GeoDict modules



www.geodict.com

FlowDict: Permeability/Flow resistivity and relative permeability

SatuDict: Capillary pressure-saturation curves

DiffuDict: Gas diffusivity

ThermoDict: Heat conductivity

ElastoDict: Elasticity tensor

FilterDict: Filtration efficiency

AcoustoDict: Acoustic properties

Effective acoustic models

Parameter	Model and type of absorber		
Flow resistivity σ [kg/m ³ s]	Delany/Bazley, Mechel Highly porous absorbers		
Porosity, Φ	Allard/Johnson Pride/Lafarge Porous with rigid frame		
Tortuosity, τ			
Viscous charact. length Λ [μ m]			
Thermal charact. length, Λ' [μ]			
Density, ρ [kg/m ³]	Biot Porous with (visco-)elastic frame		
Young's modulus E [GPa]			
Poisson's ratio, ν			
Damping loss, η			

Numerical determination of the Allard-Johnson parameters

Porosity: Given as input parameter for non-woven generation

Flow resistivity: From the flow field as the solution of the Stokes equation

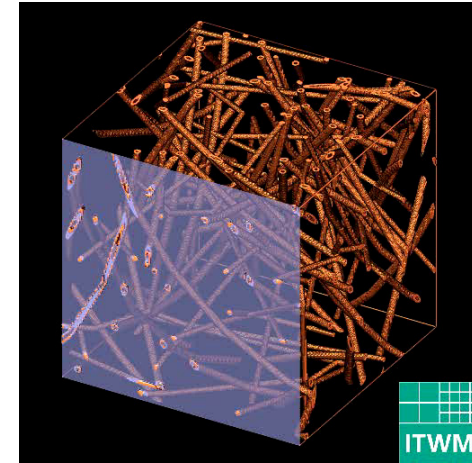
Tortuosity: Evaluation of the path length of the streamlines

$$\tau = \frac{\langle |\vec{v}| \rangle}{\langle \vec{v}_x \rangle}$$

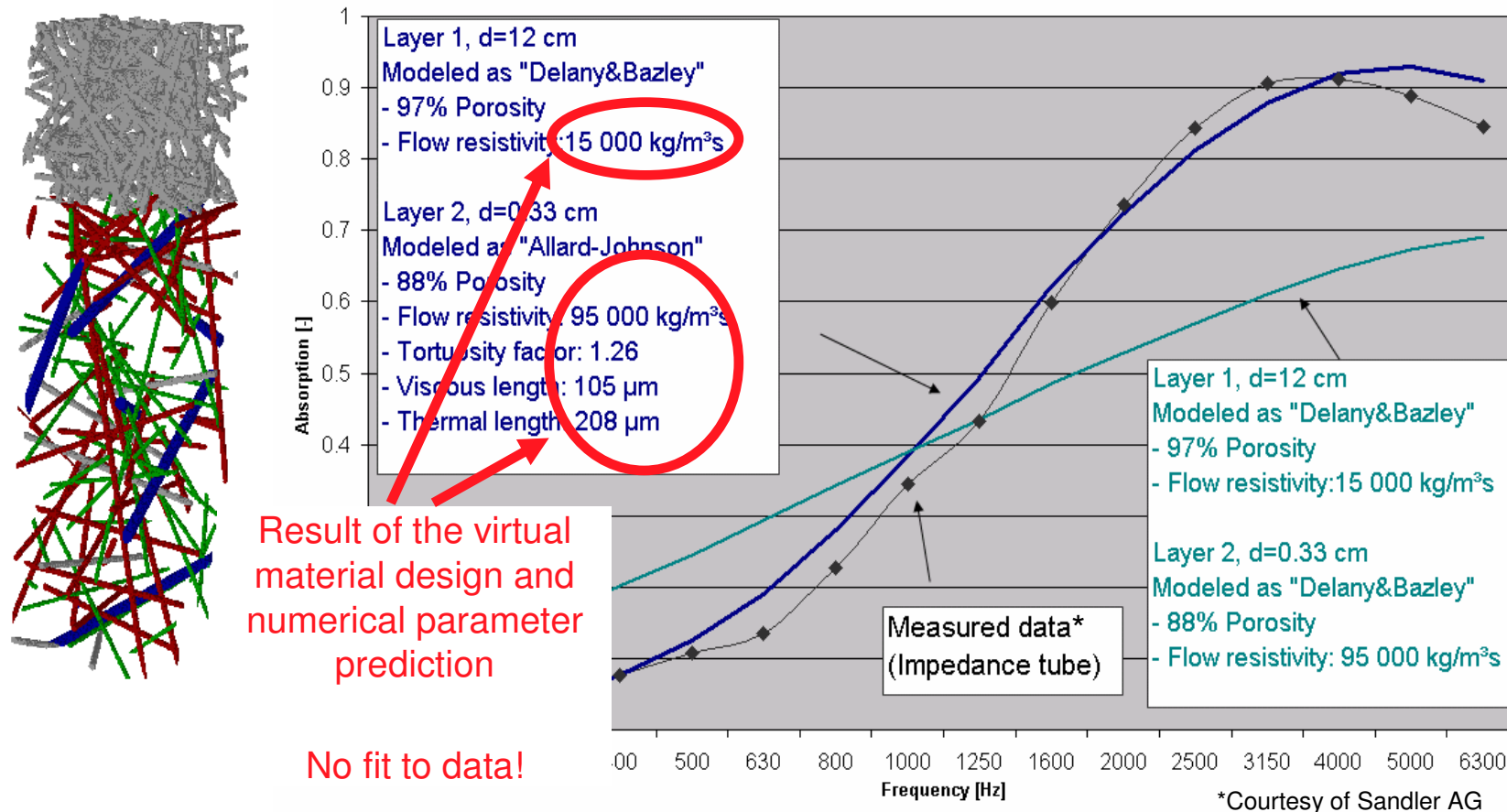
Thermal characteristic length:

$$\Lambda' = \frac{2 \cdot \text{pore volume}}{\text{fiber surface}}$$

Viscous characteristic length:

$$\Lambda \approx 0.5 \cdot \Lambda'$$


How good is our prediction?



Compression study

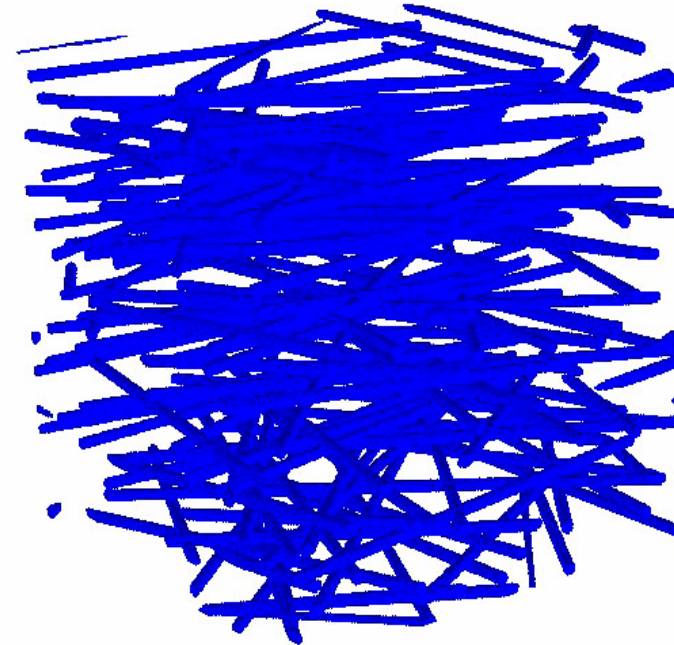
Compression of the non-woven can be used to modify the material properties in a controlled way

Example: non-woven

PET fibers, 12.15 dtex

Initial thickness 13.13 mm

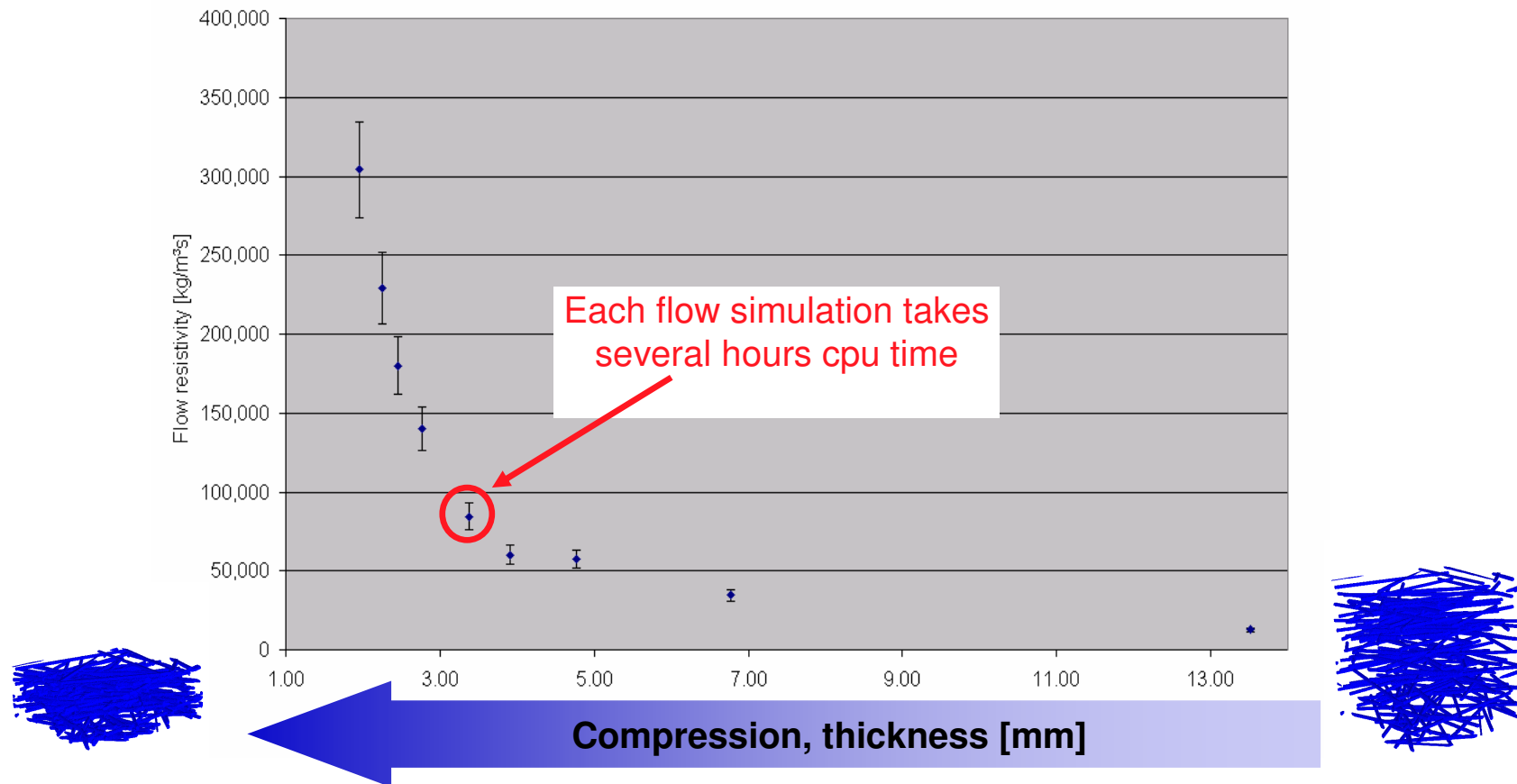
Area weight 900 g/m²



How does the microstructure change when it is compressed?

How do the material properties change under compression?

Allard-Johnson parameters versus thickness und compression



Parameterisation

Allard-Johnson parameters as a function of the porosity Φ

A_w : Area weight

ρ : Material density

d : Thickness

$$\Phi = 1 - \frac{A_w}{\rho \cdot d}$$

Flow resistivity

$$\sigma(\Phi) = \alpha \cdot \Phi^{-\beta}$$

Tortuosity

$$\tau(\Phi) = \gamma \cdot (1 - \Phi) + 1$$

Characteristic lengths

$$\Lambda'(\Phi) = \frac{1}{\delta \cdot (1 - \Phi)}$$

$$\Lambda(\Phi) = 0.5 \cdot \Lambda'(\Phi)$$

Poroacoustic material parameters, different for each non-woven

Example: 12.15 dtex PET non-woven under compression

Allard-Johnson parameters versus
thickness/porosity

Flow resistivity

$$\sigma(\Phi) = 12,834 \cdot \Phi^{-8.3548} \text{ kg/m}^3\text{s}$$

Tortuosity

$$\tau(\Phi) = 0.521 \cdot (1 - \Phi) + 1$$

Characteristic lengths

$$\Lambda'(\Phi) = 0.0673^{-1} \cdot (1 - \Phi)^{-1} \mu\text{m}$$

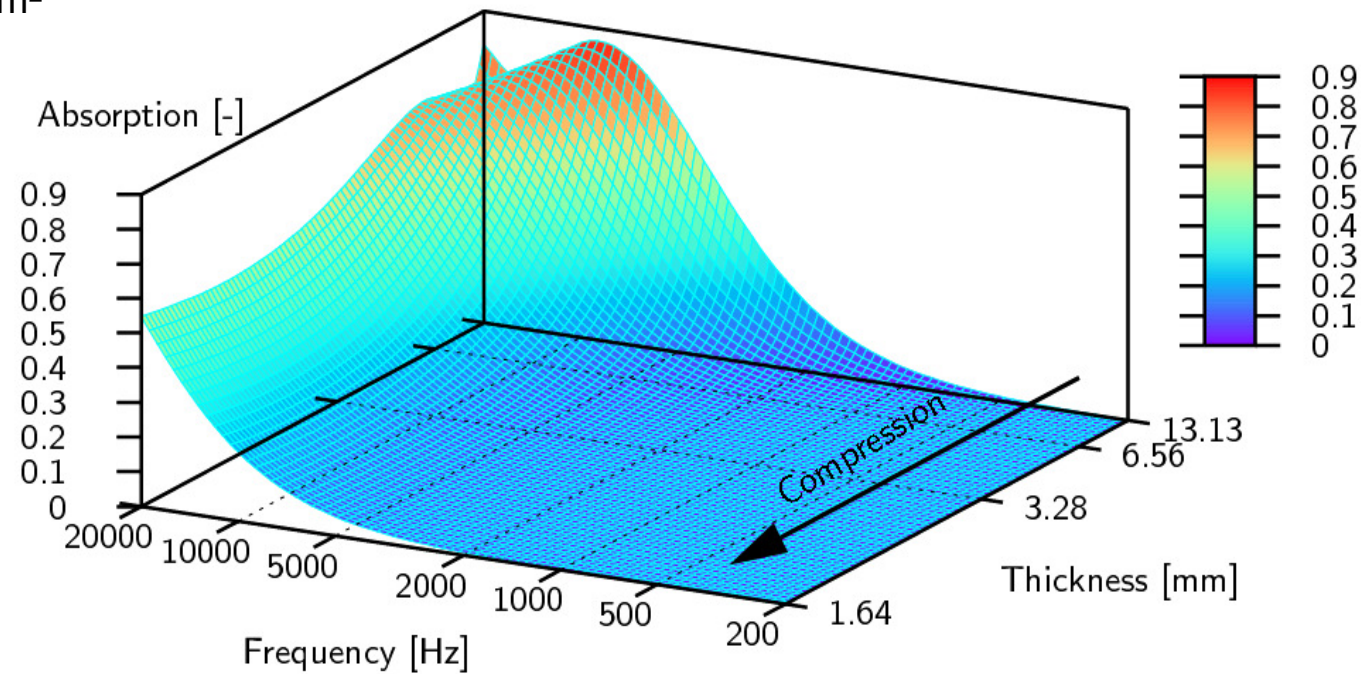
$$\Lambda(\Phi) = 0.5 \cdot \Lambda'(\Phi) \mu\text{m}$$

Poroacoustic material
parameters:
Complete description of
the acoustic properties of
the compressed non-
woven

Acoustic absorption

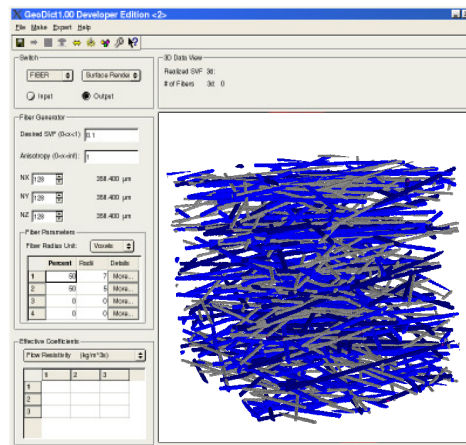
12.15 dtex PET

Area weight 900 g/m²

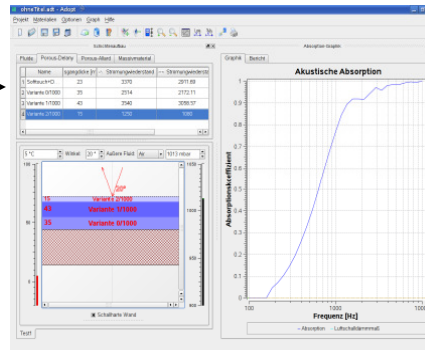


AdOpt: Acoustic database and optimization tool

GeoDict+AcoustoDict



AdOpt



Prediction of acoustic

- Impedance
- Transmission Loss
- Absorption

for **layered** materials

Material database

- Fiber parameters
- Poroacoustic material parameters

Optimal material selection

Export to acoustic simulation software:

- AutoSEA2, Ansys, SysNoise, ...

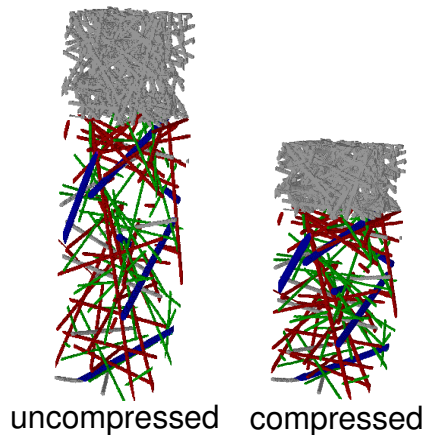
Summary

Without prototyping we predict the acoustic properties of uncompressed and compressed layered non-wovens

Step 1: **GeoDict**

Microstructure generation based on

- Fiber diameters
- Area weight
- Anisotropy
- ...



Step 2: **AcoustoDict**

Numerical determination:

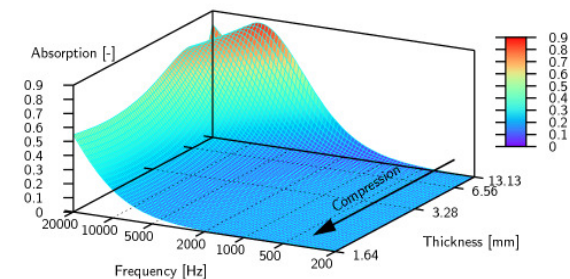
- Flow resistivity
- Tortuosity
- Characteristic lengths

⇒ Poroacoustic material parameters

Step 3: **AdOpt**

Prediction of acoustic absorption, transmission loss, etc. for layered structures

Arbitrary parameter variation possible (number of layers, thickness, compression)



Outlook

Extended validation of the method is on the way

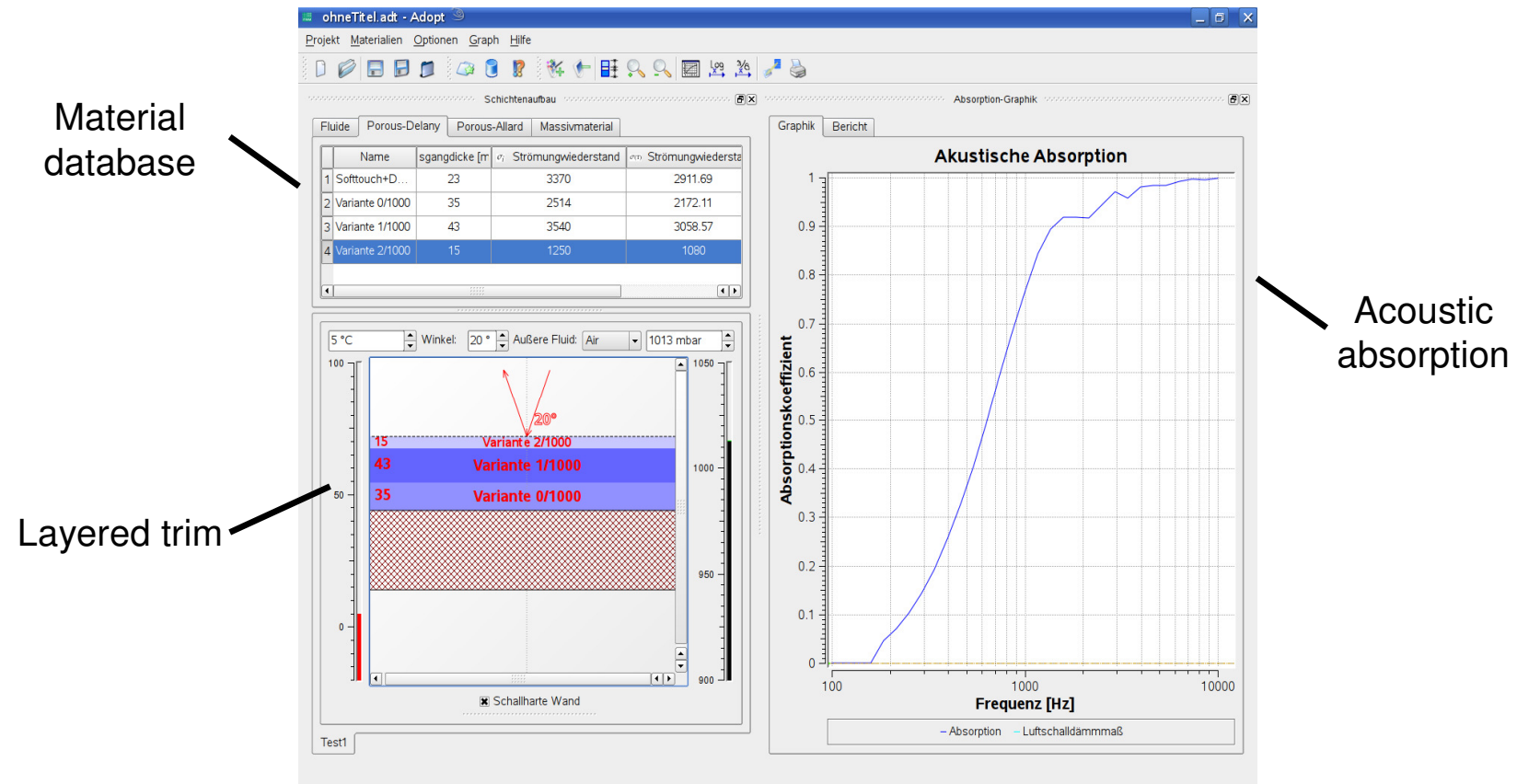
Numerical determination of the viscous characteristic length (instead of $\Lambda \approx 0.5 \Lambda'$)

Application to other porous absorbers such as wovens or metal foams

Extension to porous absorbers with (visco-)elastic frame (,foams')
⇒ numerical determination of the Biot parameters

Ongoing software development

AcoustoDict and AdOpt will be available Fall 2007



AdOpt: Screenshot of the developer version

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Techtextil 3.0 H16

