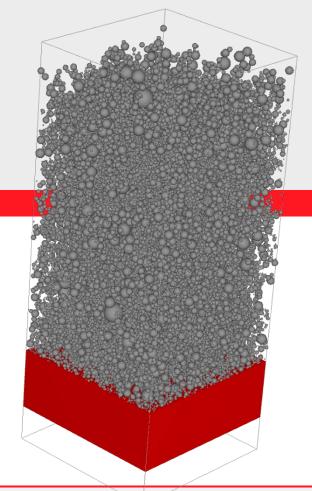
# From Resolved Filtration Simulations to Effective Cake Filtration Simulation Parameters

AFS Fall Conference 2016 San Diego, CA Oct 25<sup>th</sup>, 2016

#### **Liping Cheng**

Sven Linden Jürgen Becker Cornelia Kronsbein Andreas Wiegmann





#### Math2Market GmbH

### Some background information

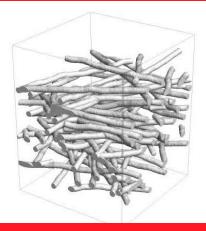
- Math2Market creates and markets software for engineers and scientists that want to analyze and design porous and composite materials based on the material's geometric inhomogeneity.
- The materials can come from µCT, FIB-SEM or models and are represented as 3-dimensional images in the software.
- This software is called GeoDict, the Digital Material Laboratory.
- M2M is based in Kaiserslautern, Germany.
- M2M spun off from Fraunhofer Institute for Industrial Mathematics.

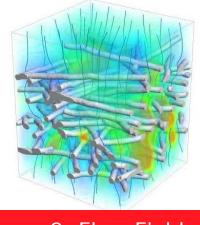
Visit us at our booth

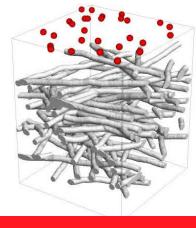




### How is cake filtration simulated?



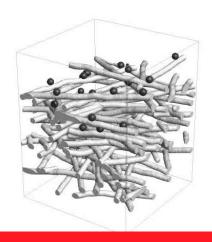


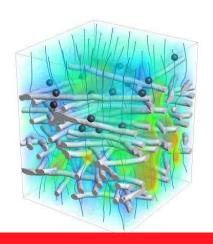


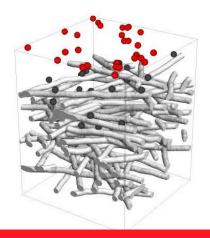
1. Filter Model

2. Flow Field

3. Track Particles







4. Deposit Particles

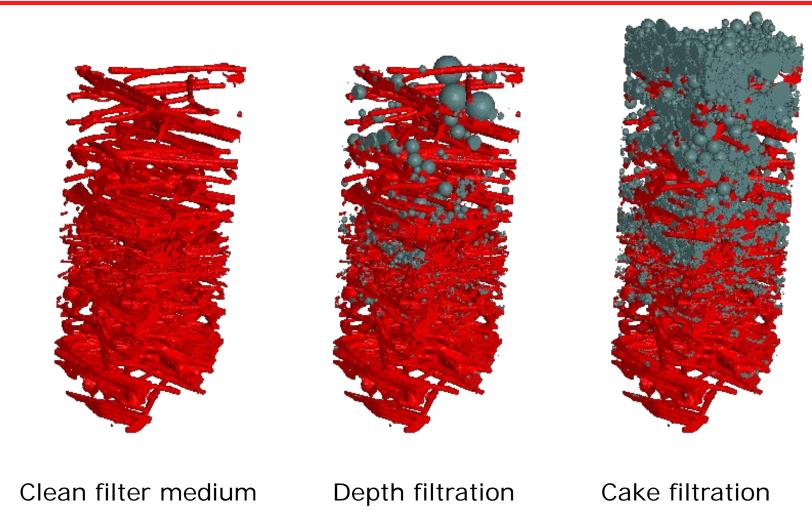
5. Flow Field

6. Repeat ...



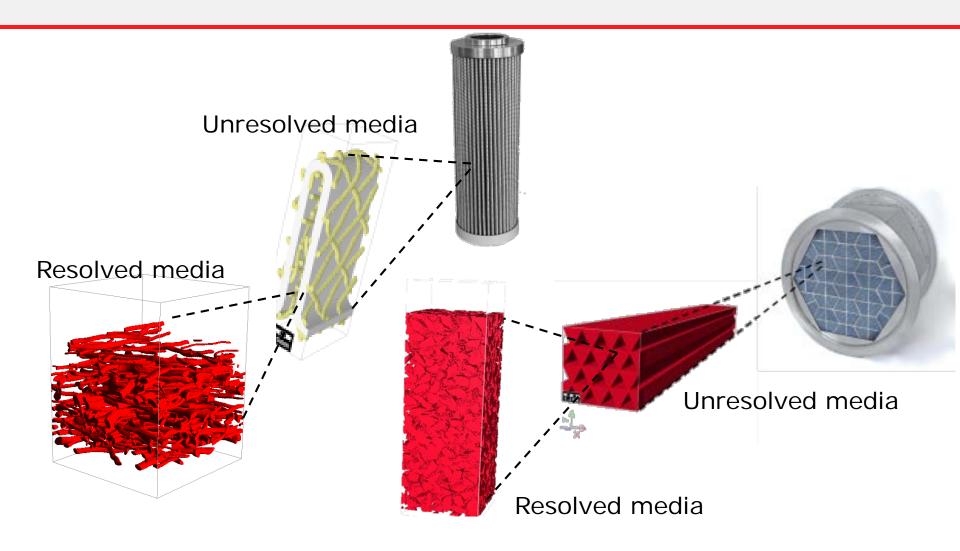


# Depth filtration vs. cake filtration





### Resolution: filter media







# **Resolution: particles**

Particles Domain	Unresolved	Mixed	Resolved
Media Scale			
A STATE OF THE STA			
Pleat / DPF Scale			





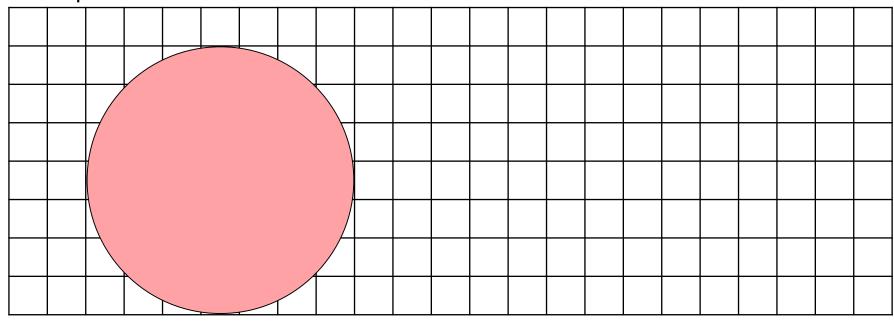
### Scale Issue of Cake Filtration Simulation on Uniform 3d Grids

- When all particles are much larger than the grid size, then solid and empty cells suffice to represent them.
- When all particles are much smaller than the computational grid size, then an homogeneous porous media approach works.
- Resolved and unresolved particles are both present in the polydisperse particles.
- When the particle size distribution includes larger particles and smaller particles than the grid size, then sub-grid resolution and parameters for inhomogeneous porous media are required.
- We describe two approaches to find these parameters.



# Computational Grid, Resolved

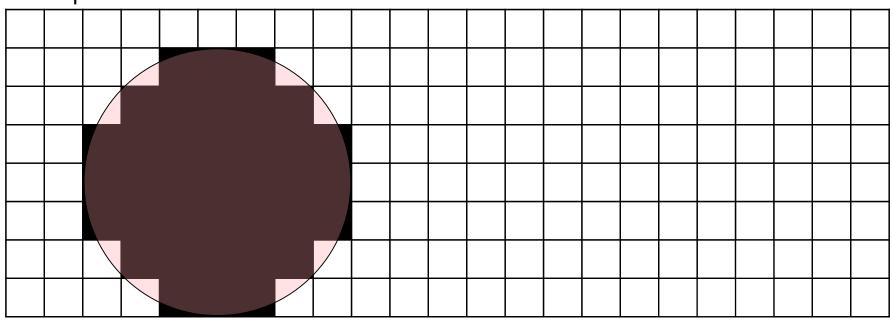
# Computational Grid



**Resolved Particle** 

### **Discretization of Resolved Particles**

### Computational Grid



**Resolved Particle** 

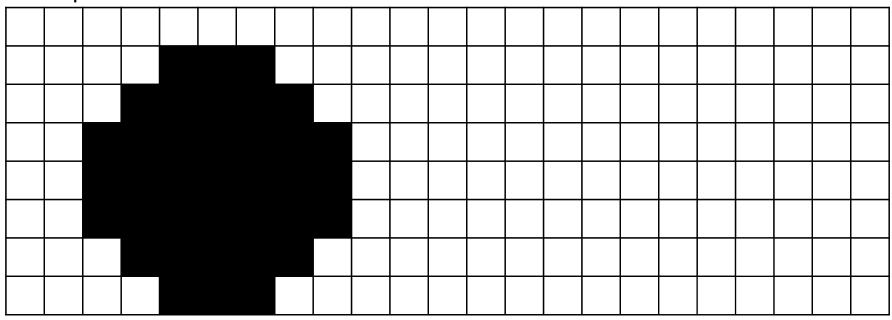
Empty/Solid Cells





### **Discretization of Resolved Particles**

### Computational Grid



**Resolved Particle** 

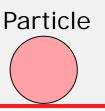
Empty/Solid Cells











- Voxels are solid or empty
- Stationary incompressible Navier-Stokes equation

$$-\mu\Delta\vec{u} + \rho(\vec{u}\cdot\nabla)\vec{u} + \nabla p = 0, \qquad \nabla\cdot\vec{u} = 0$$

$$\mu$$
 viscosity  $\rho$  density  $u$  velocity  $p$  pressure

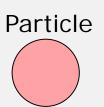
Particles are discretized into solid/empty grid cells

Output parameters:  $f_{max}$  (maximal solid volume fraction) and  $\sigma_{max}$  (maximal flow resistivity)

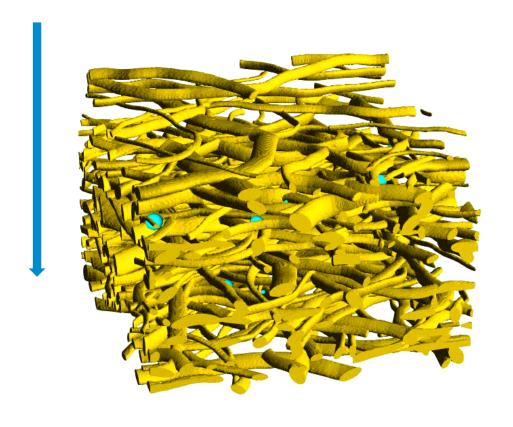


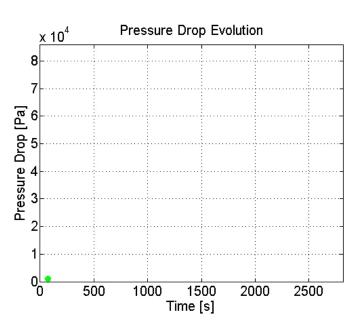






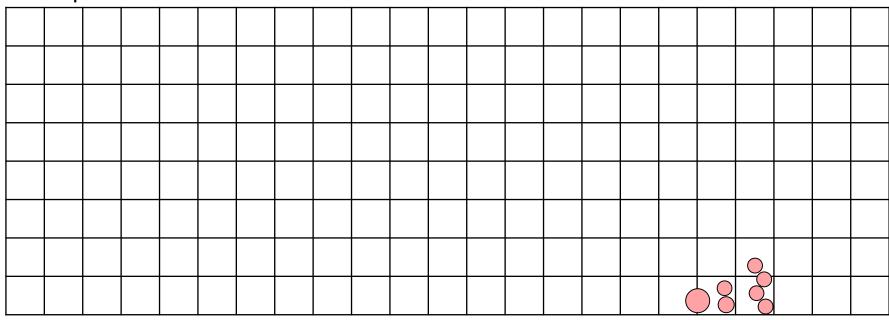
Example: Oil filtration – Multi Pass test; sieving model





# **Computational Unresolved Particles**

### Computational Grid

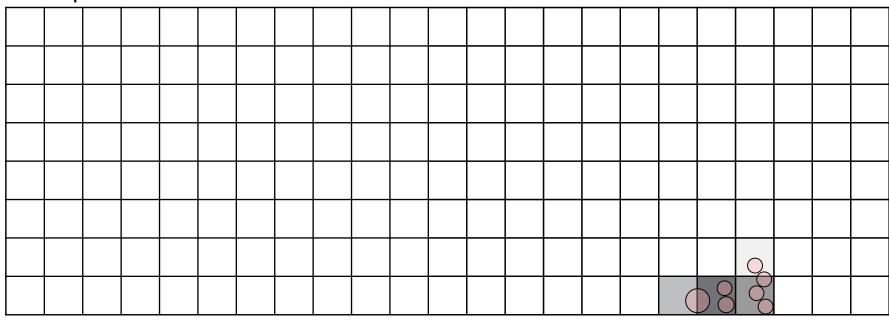


**Unresolved Particles** 



### Discretization of Resolved and Unresolved Particles

### Computational Grid



**Unresolved Particles** 

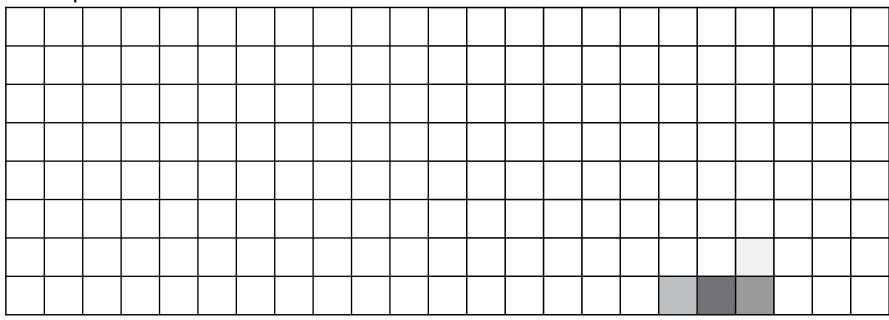
Porous Cells





### Discretization of Resolved and Unresolved Particles

### Computational Grid



**Unresolved Particles** 

Porous Cells





# **Unresolved Particles**









- Voxels are solid, empty or porous
- Stationary incompressible Navier-Stokes-Brinkman equation

$$-\mu\Delta\vec{u} + \rho(\vec{u}\cdot\nabla)\vec{u} + \sigma\vec{u} + \nabla p = 0, \qquad \nabla\cdot\vec{u} = 0$$

$$\nabla \cdot \vec{u} = 0$$

σ: resistivity

In porous voxels:

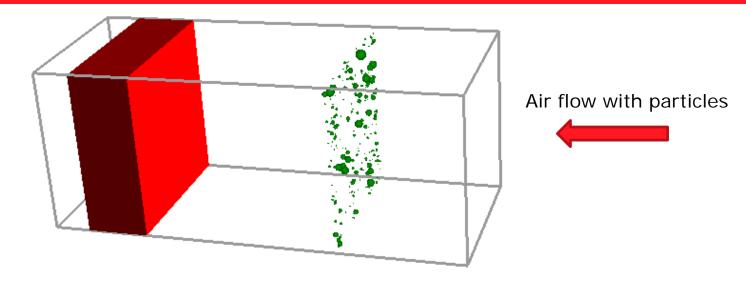
- Local solidity f changes when a particle is added.
- When  $f_{max}$  is reached, no more particles can be added.
- Local flow resistivity:

$$\sigma = \begin{cases} \frac{f}{f_{max}} \sigma_{max} & \text{for } 0 < f < f_{max} \\ \sigma_{max} & \text{for } f_{max} \le f \le 1 \end{cases}$$

**SVF**  $\sigma_{max}$  $f_{max}$ 

Input parameters:  $f_{max}$  (maximal solid volume fraction) and  $\sigma_{max}$  (maximal flow resistivity)

# **Simulation Setup**

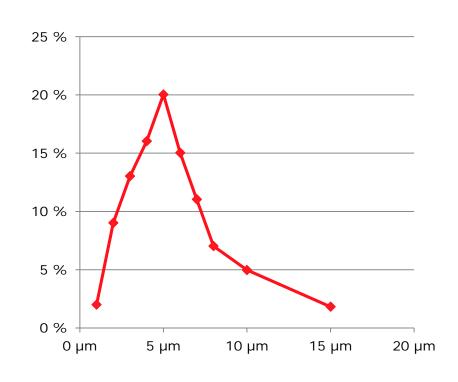


- No depth filtration, only cake filtration
- Unresolved filter media: 48 µm thick, fixed permeability
- Particles are caught on first touch
- Particle diameter range between 1µm and 15µm
- 1. Vary resolution between 0.5 µm per voxel and 24 µm per voxel
- 2. Determine flow resistivity and cake solidity



### **Particle Size Distribution**

Particle Diameter	Mass %	Count %	
1 µm	2.00	48.340	
2 µm	9.01	27.190	
3 µm	13.03	11.640	
4 µm	16.04	6.040	
5 µm	20.04	3.870	
6 µm	15.03	1.680	
7 µm	11.03	0.780	
8 µm	7.03	0.330	
10 µm	4.97	0.120	
15 µm	1.82	0.013	

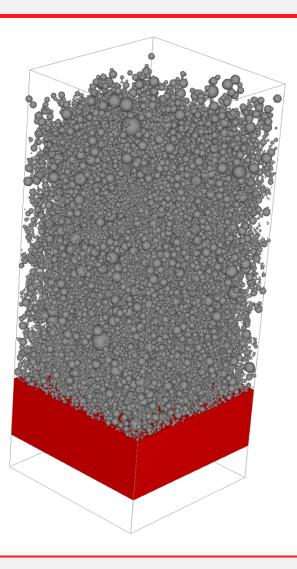


SAE Ultrafine Dust (ISO 12103-1)





#### **Resolved Particles**

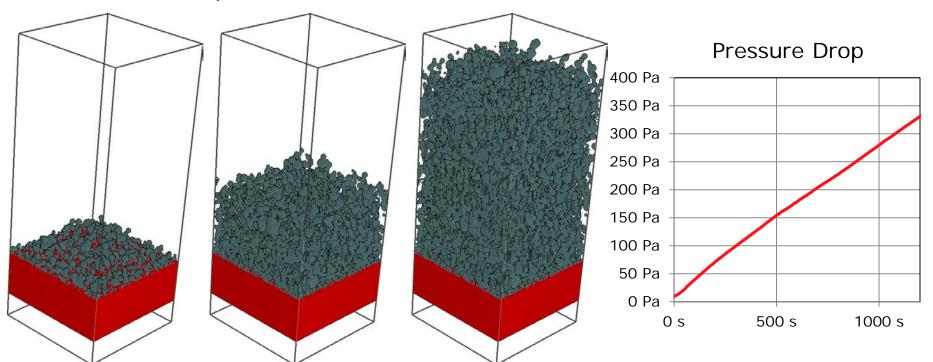


- Simulation with all resolved particle works by entering them as solid / empty and computing Stokes flow in the pores.
- The solid volume fraction  $f_{max}$  and the resistivity  $\sigma_{max}$  agrees to the experimental cake valules  $f_{real}$  and  $\sigma_{real}$ .



# Resolved Particles Caught On First Touch

# Resolution 0.5µm



#### Result:

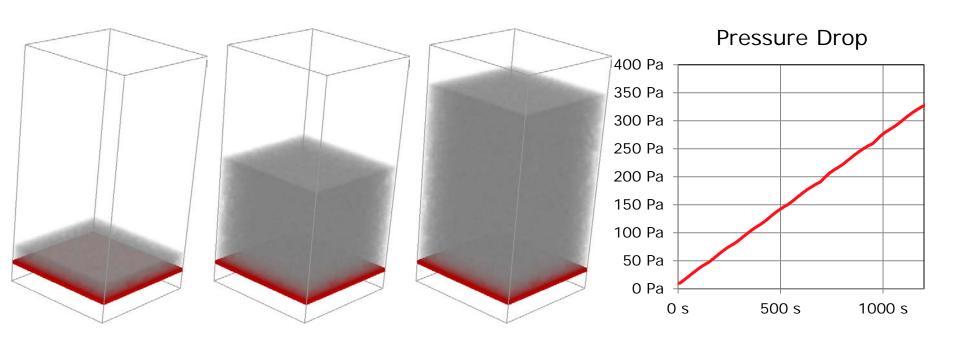
- Flow resistivity 14.4 e+6 kg/m³s
- Cake solidity 0.1953





# Fully Unresolved Particles Caught On First Touch

### Resolution 24µm



Input (porous voxels):

 $\sigma_{max} = 14.4 \text{ e} + 6 \text{ kg/m}^3 \text{s}$ 

 $f_{max} = 0.1953$ 

#### Result:

- Flow resistivity 14.3 e+6 kg/m³s
- Cake solidity 0.2027





# Unresolved Particles resolved media





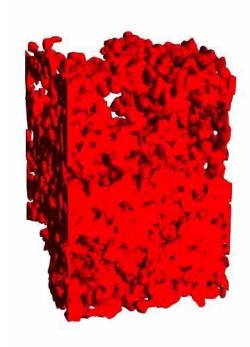




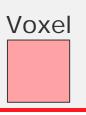
Example: Soot filtration – ceramic filter; caught on first touch model







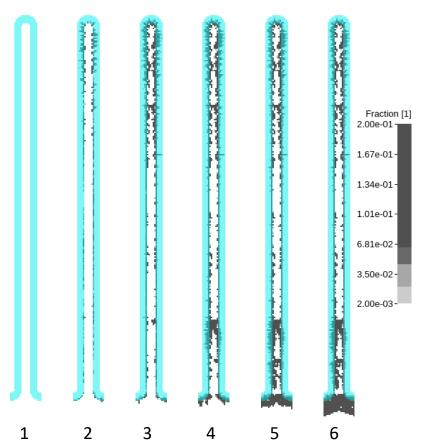
## **Unresolved Particles** unresolved media



Fiber

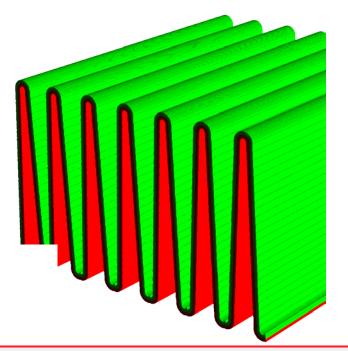


Particle



Filter material described by

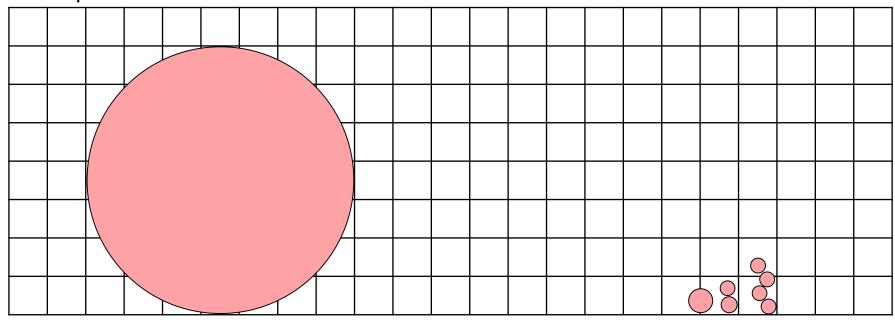
- porosity
- permeability
- capturing probability model





# Computational Grid, Resolved & Unresolved Particles

### Computational Grid



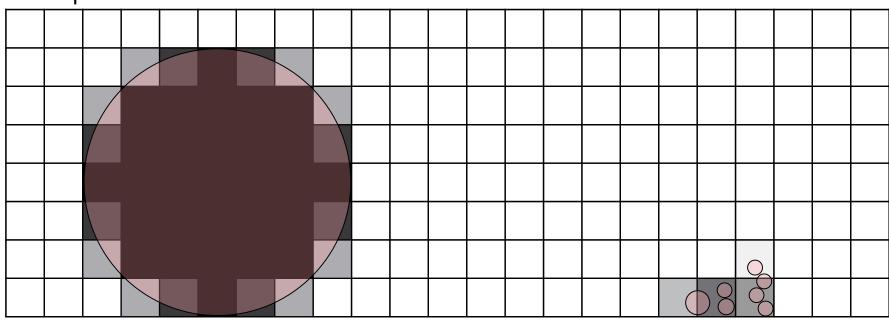
**Resolved Particle** 

**Unresolved Particles** 



#### Discretization of Resolved and Unresolved Particles

### Computational Grid



**Resolved Particle** 

**Unresolved Particles** 

Empty/Solid/porous Cells

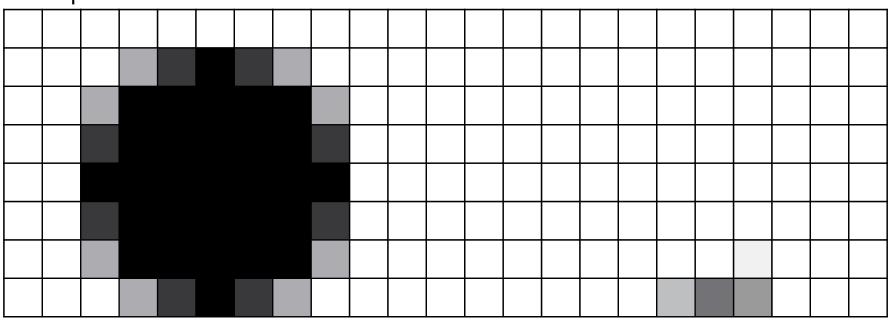
Porous Cells





#### Discretization of Resolved and Unresolved Particles

### Computational Grid



**Resolved Particle** 

**Unresolved Particles** 

Empty/Solid/porous Cells

Porous Cells





### **Resolved and Unresolved Particles**

- Particles turn voxels into solid or porous.
- Stationary incompressible Navier-Stokes-Brinkman equation

### In porous voxels:

Local flow resistivity:

$$\sigma = \begin{cases} \frac{f}{f_{max}} \sigma_{max} & \text{for } 0 < f < f_{max} \\ \sigma_{max} & \text{for } f_{max} \le f \le 1 \\ \infty & \text{for } f = 1 \end{cases}$$

Input parameters:  $f_{max}$  (maximal solid volume fraction) and  $\sigma_{max}$  (maximal flow resistivity)



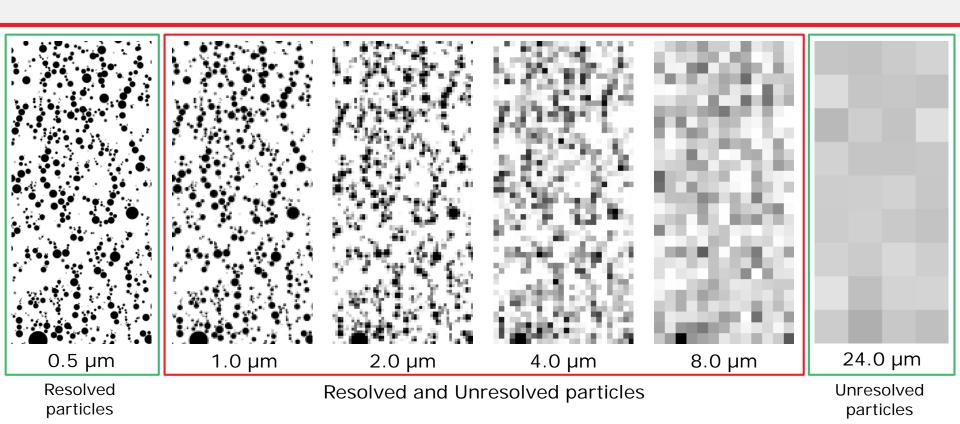
# Fully Resolved vs. Fully Unresolved particles

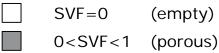


 $\square$  SVF=0 (empty)  $\square$  0<SVF<1 (porous)



# Mixed Resolved & Unresolved particles for varying resolutions









# Results for Partially Resolved particles with parameters for Unresolved particles

Resolution	Input pa	rameters	Resulting cake		
	f <sub>max</sub>	σ <sub>max</sub> [10 <sup>6</sup> kg/m <sup>3</sup> s]	Solidity	Flow resistivity [10 <sup>6</sup> kg/m³s]	
24 µm	0.1953	14.4	0.2027	14.30	
0.5 µm	solid/empty	solid/empty	0.1953	14.40	





30

# Results for Partially Resolved particles with parameters for Unresolved particles

Resolution	Input pa	rameters	rs Resulti		ltir	ing cake		
	f <sub>max</sub>	σ <sub>max</sub> [10 <sup>6</sup> kg/m <sup>3</sup> s]		Solidity		Flow resistivity [10 <sup>6</sup> kg/m³s]		
24 µm	0.1953	14.4		0.2027			14.30	
8 µm	0.1953	14.4		0.1953			10.17	
4 µm	0.1953	14.4		0.1422			4.02	
2 μm	0.1953	14.4		0.1346			3.09	
1 µm	0.1953	14.4		0.1535			4.41	
0.5 µm	solid/empty	solid/empty		0.1953			14.40	

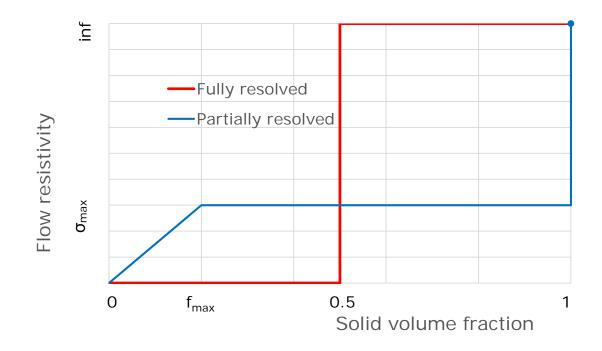
Solidity too low Need higher  $f_{max}$ 

Resistivity too low Need higher  $\sigma_{max}$ 





# Results for Partially Resolved particles with parameters for Unresolved particles



# **Quick parameter fitting**

Resolution 4 µm		Input p	parameters	Resulting cake		
		f <sub>max</sub>	σ <sub>max</sub> [10 <sup>6</sup> kg/m <sup>3</sup> s]	Solidity	Flow resistivity [10 <sup>6</sup> kg/m³s]	
Use result of resolved model		0.1953	14.40	0.1422	4.02	
2. Use other values		0.4000	200.00	0.2505	50.00	





# **Quick parameter fitting**

Resolution 4 µm	Input	parameters	Resulting cake		
	f <sub>max</sub>	σ <sub>max</sub> [10 <sup>6</sup> kg/m <sup>3</sup> s]	Solidity	Flow resistivity [10 <sup>6</sup> kg/m³s]	
1. Use result of resolved model	0.1953	14.40	0.1422	4.02	
3. Assume linear dependency solidity from $f_{max}$ $\Longrightarrow$ resistivity from $\sigma_{max}$	0.2956	56.34	0.1904	13.50	
2. Use other values	0.4000	200.00	0.2505	50.00	





# Results for mixed resolutions with fitted parameters

Resolution	Input pa	rameters	Resulting cake		
	f <sub>max</sub>	σ <sub>max</sub> [10 <sup>6</sup> kg/m <sup>3</sup> s]	Solidity	Flow resistivity [10 <sup>6</sup> kg/m³s]	
24 µm	0.1953	14.4	0.2027	14.3	
8 µm	0.1953	20.19	0.1967	14.4	
4 μm	0.2956	56.34	0.1904	13.5	
2 μm	0.4600	170.00	0.1949	13.8	
1 µm	0.5000	441.50	0.1928	15.2	
0.5 µm	solid/empty	solid/empty	0.1953	14.4	





# **Summary of previous work**

- Solidity and flow resistivity of a filter cake can be modeled by
  - Simulating one cake filtration with fully resolved particles
  - Simulating two cake filtrations with partly resolved particles
  - Parameter fitting

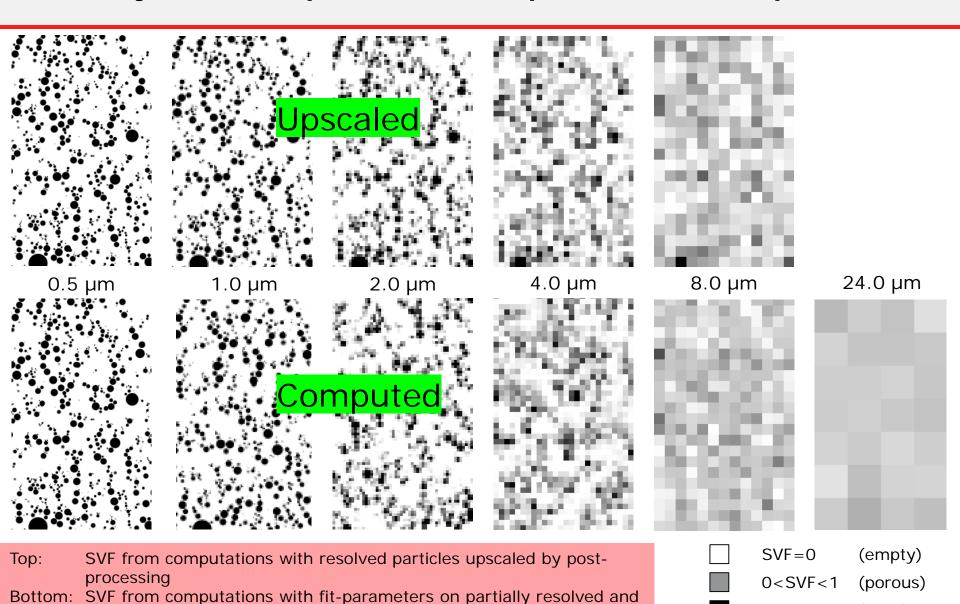
### **Questions:**

- Do local solidity and local flow resistivity distributions match for resolved and mixed resolution computations?
- Can we estimate  $f_{max}$  and  $\sigma_{max}$  from just a single resolved cake filtration simulation?
  - Reduce estimation effort from three to one simulation
  - Develop a theory or provide a data base with effective parameters depending on particle size distribution and grid resolutions
- A methodology to measure *local solidity* and *local flow resistivity* on square blocks of  $1\times1\times1$ ,  $2\times2\times2$ ,  $4\times4\times4$  cells with the finest resolution results (0.5µm)
  - $1 \times 1 \times 1 -> 0.5 \mu m$
  - 2×2×2 -> 1.0µm
  - $\blacksquare$  4×4×4 -> 2.0µm





# Comparison: Computations with Resolved particles vs. Partially Resolved particles and up to Unresolved particles

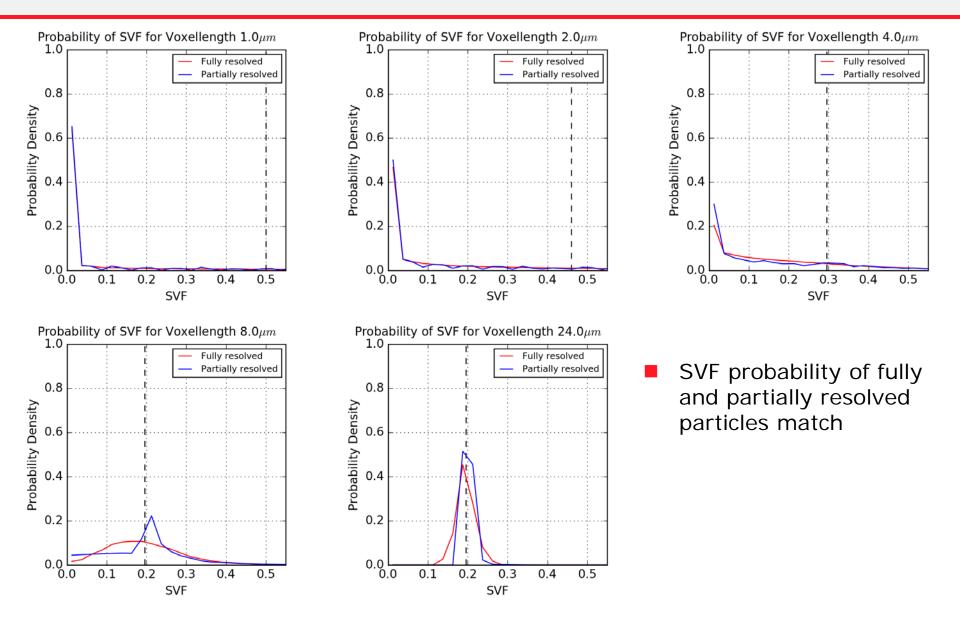


unresolved particles

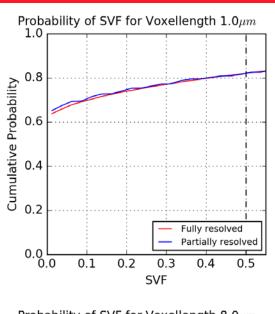
SVF = 1

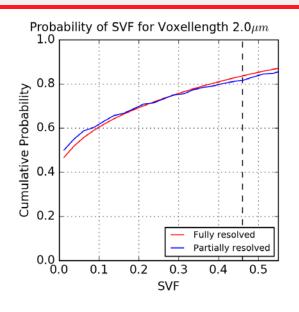
(solid)

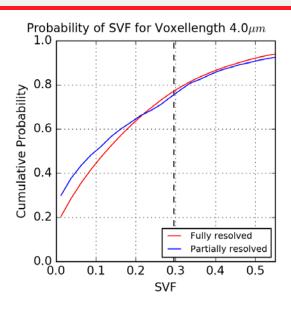
### Comparison of SVF probability density

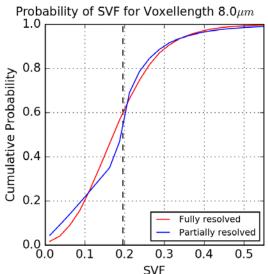


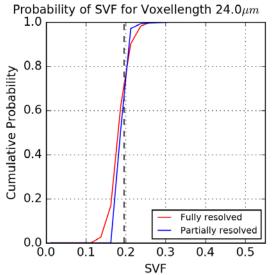
### Comparison of SVF cumulative probability











- SVF probability of Fully and Partially Resolved particles match
- Cumulative probability between 60% and 80% at  $f_{max}$

### **Conclusions and outlook**

- Cake formation can be modeled at different resolutions
- Parameters  $f_{max}$  and  $\sigma_{max}$  can be estimated by linear fitting
- Local solidity and flow resistivity of Fully Resolved and Partially Resolved computations match
- The  $\sigma$  function for different resolutions can be estimated from Fully Resolved computations
- Open questions:
  - How to estimate  $f_{max}$  from one Fully Resolved cake filtration?
  - Can the  $f_{max}$ ,  $\sigma_{max}$  model be replaced?



# **GEODICT**

The Digital Material Laboratory

#### **Standard Edition**

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Dr. Christian Wagner, Dr. Rolf Westerteiger,
Nicolas Harttig, Andreas Grießer,
and Andreas Wiegmann, PhD

Art Design: Steffen Schwichow

















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