# The Influence of Variable Wettability on Mass Transport Properties of GDLs

Jürgen Becker, Christian Wagner, Sven Linden, Andreas Wiegmann

ModVal Lausanne, 23.03.2016

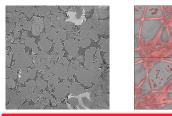


#### Who is Math2Market?

- Math2Market GmbH was founded 2011 in Kaiserslautern.
- Spin-off of Fraunhofer Institute for Industrial Mathematics, ITWM.
- Today: 12 full-time, 6 part-time employees, turnover >2 Mio € / year
- Our product: GeoDict software
  - Sales
  - Development and Customization
  - Consulting



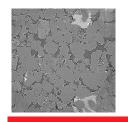






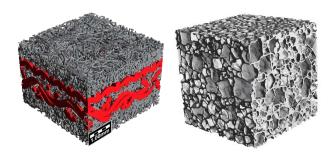
Import of CT Scans





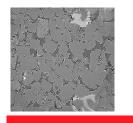


Import of CT Scans



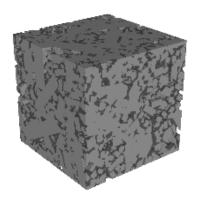
Create 3D Models of Microstructures







Import of CT Scans

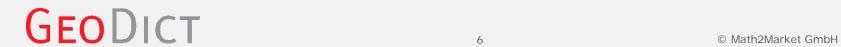


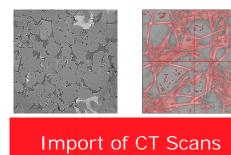
Geometric Analysis of 3D Structures

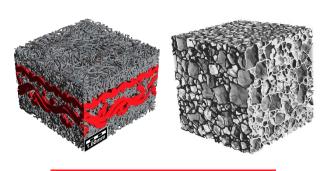




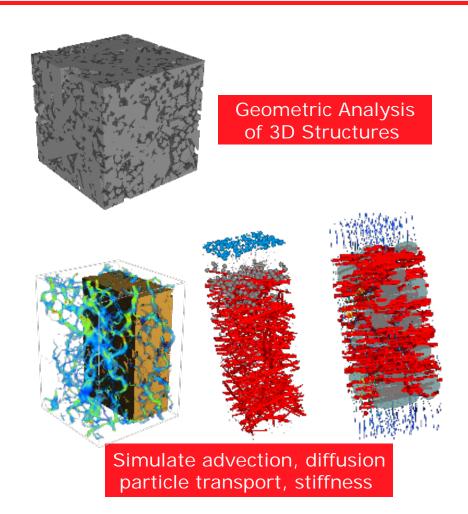
Create 3D Models of Microstructures







Create 3D Models of Microstructures



#### ... with applications in:

Filtration

Mostly automotive, filter media & filters

Personal Care

Wipes, Feminine Care, Baby Care

Electrochemistry

Fuel cell media & battery materials

Weaves and Paper

Paper forming and dewatering, Metal Wire Mesh

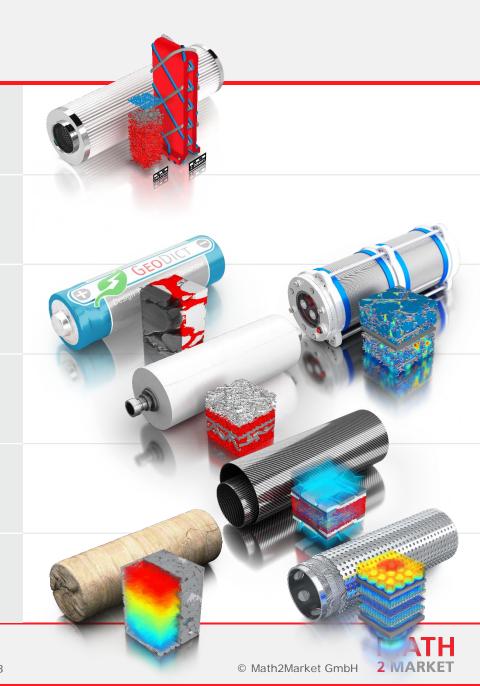
Composites

Mostly automotive, lightweight materials

Oil and Gas

Digital rock physics, digital sand control





# The Influence of Variable Wettability on Mass Transport Properties of GDLs

#### Overview:

- 1. 3D GDL model and compression
- 2. Computing permeability
- 3. Capillary pressure and saturation with variable wettability
- 4. Effect on relative permeability



# 3D GDL Model and Compression





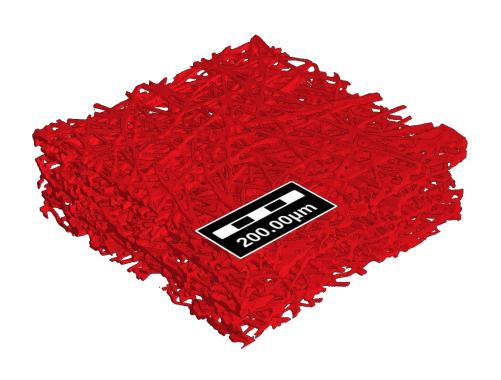
#### **Structure Model**

#### GDL:

- Carbon fibers, 7 µm diameter
- 20 wt% binder
- 200 µm thickness

#### Model

- 1 µm resolution
- Voxel grid
- 600x600x200 = 72 Mio. cells
- Stochastic process



Fibers: linear elastic, transverse isotropic

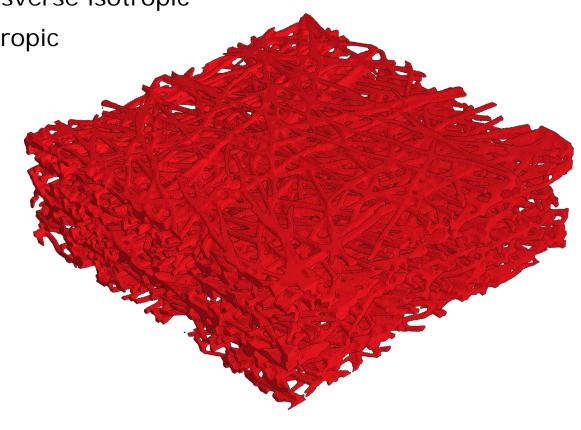
Binder: linear elastic, isotropic

Solver:





Runtime: 1h 17 min (8x)



Compression

0

0.05

0.1

0.15

0.2





Fibers: linear elastic, transverse isotropic

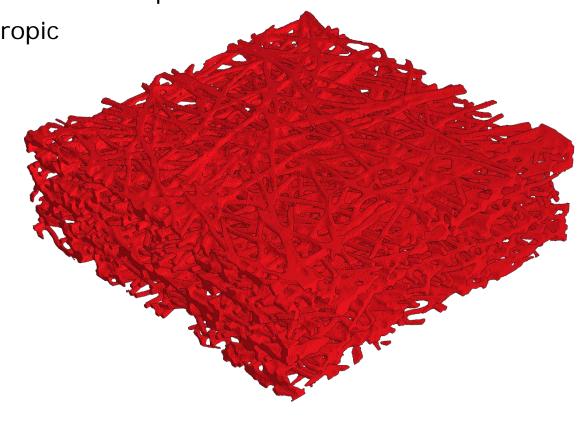
Binder: linear elastic, isotropic

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Compression

0

0.05

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0.15

0.2



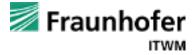


Fibers: linear elastic, transverse isotropic

Binder: linear elastic, isotropic

Solver:





Runtime: 1h 17 min (8x)



Compression

C

0.05

0.1

0.15

0.2





Fibers: linear elastic, transverse isotropic

Binder: linear elastic, isotropic

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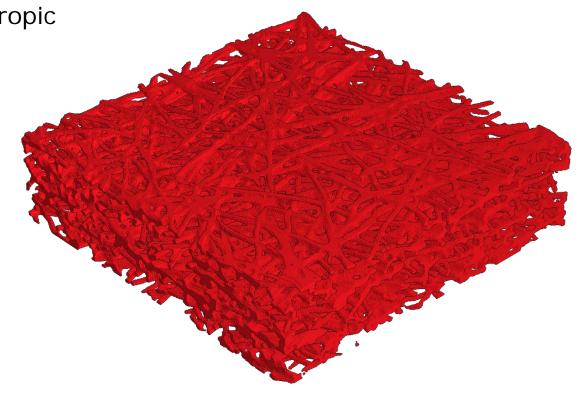
Binder: linear elastic, isotropic

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Fibers: linear elastic, transverse isotropic

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C

0.05

0.1

0.15

0.2





### **Computing Permeability**

Flow solver finds interstitial flow field **u**.

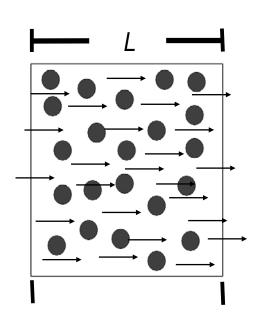
 $\overline{\mathbf{u}}$ : Average (superficial) flow velocity

 $P_1$ : Pressure average over inflow plain

 $P_2$ : Pressure average over outflow plain

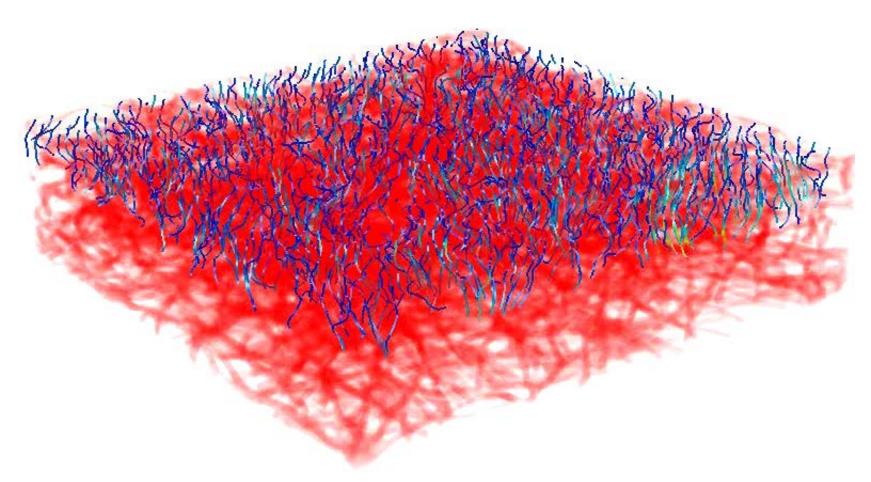
**K**: Permeability tensor

Darcy-Law: 
$$\overline{\mathbf{u}} = -\frac{\mathbf{K}}{\mu} \frac{(P_2 - P_1)}{L}$$



Pressure P<sub>1</sub> Pressure P<sub>2</sub>

#### Flow Simulation

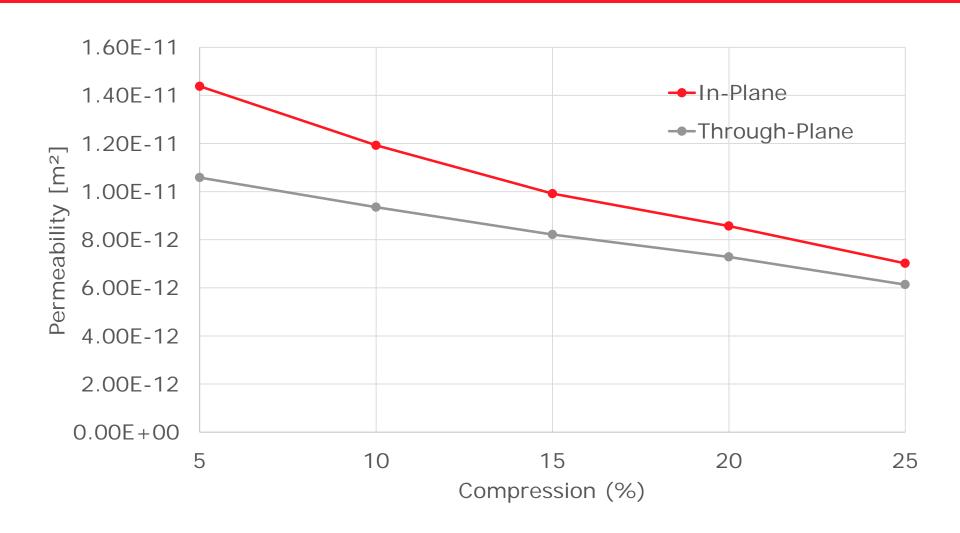


Solver runtime (12x parallel): 5 min 41 s





### **Compression and Permeability**







# Capillary Pressure and Saturation with Variable Wettability





# **Capillary Pressure**

When does the gas enter a cylindrical capillary?

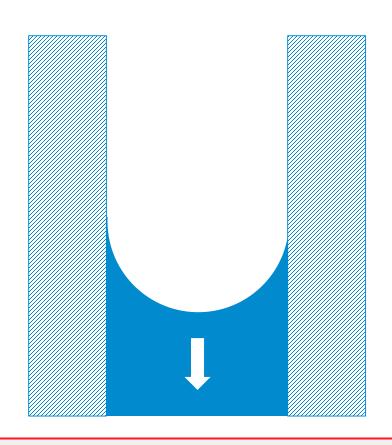
$$p = \frac{4 c}{d}$$

p differential pressure

d pore diameter

 $\sigma$  surface tension

complete wetting  $\beta = 0$ 



### **Capillary Pressure**

When does the gas enter a cylindrical capillary?

$$p = \frac{4 \sigma}{d} \cos \beta$$

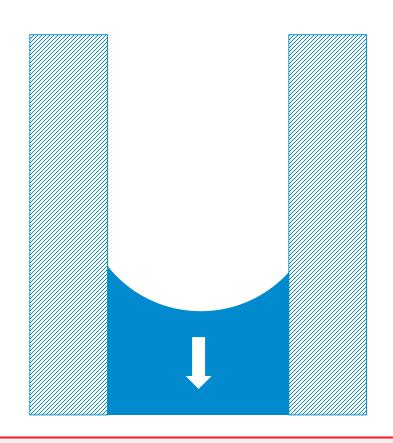
p differential pressure

d pore diameter

 $\sigma$  surface tension

 $\beta$  contact angle

partial wetting  $0^{\circ} < \beta < 90^{\circ}$ 



#### Can we have variable contact angles?

Idea (Schulz et al, 2014)

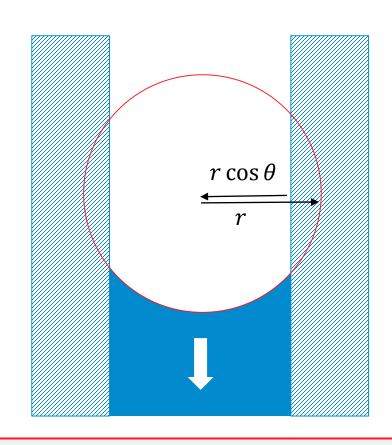
- dilate by  $r \cos \theta$
- erode by r

Result: contact angle  $\theta$  on pore wall

Young-Laplace: 
$$p = \frac{2 \sigma}{r}$$

r: sphere radius (≠ pore radius)

V.P. Schulz, E. A. Wargo, E. Kumbur, Pore-Morphology-Based Simulation of Drainage in Porous Media Featuring a Locally Variable Contact Angle, <u>Transport in Porous Media</u>, 2014.

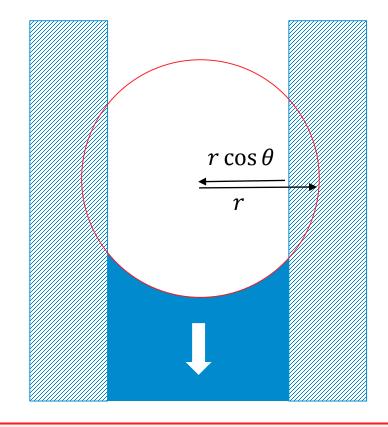


#### Can we have variable contact angles?

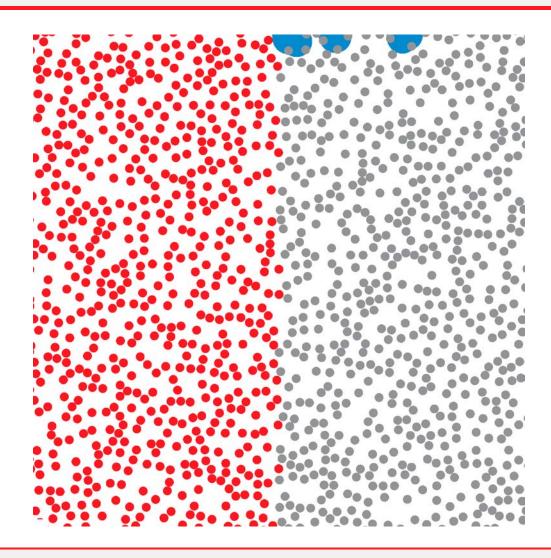
#### Restriction on possible contact angles:

- If the difference between  $r\cos\theta$  and r is larger than the fiber diameter (or wall thickness), the method produces artifacts.
  - ⇒ Contact angles should not be too close to 90°
- No mixed (hydrophobic-hydrophilic) wettability possible.

V.P. Schulz, E. A. Wargo, E. Kumbur, Pore-Morphology-Based Simulation of Drainage in Porous Media Featuring a Locally Variable Contact Angle, <u>Transport in Porous Media</u>, 2014.

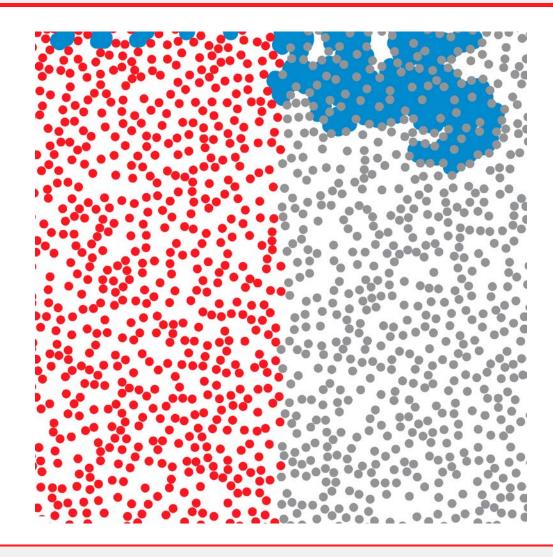


- Contact angle 0°
- Contact angle 40°
- Water (non-wetting)
- Air (wetting)

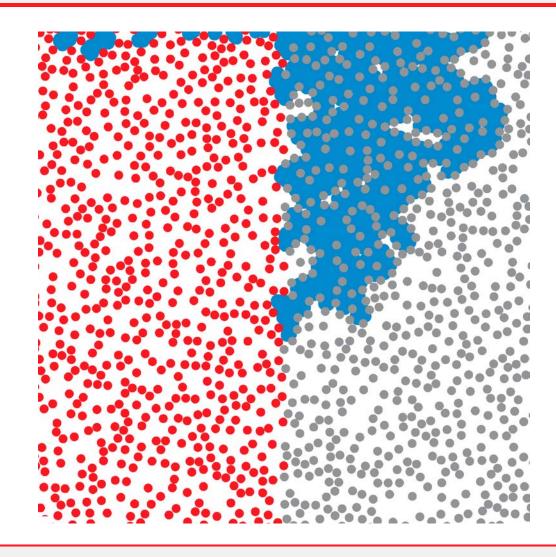




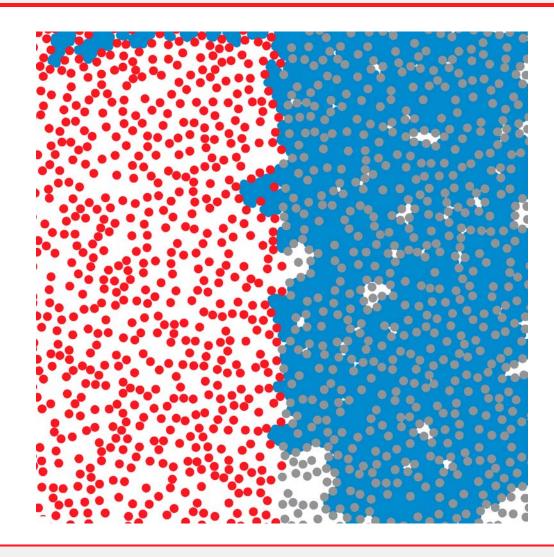
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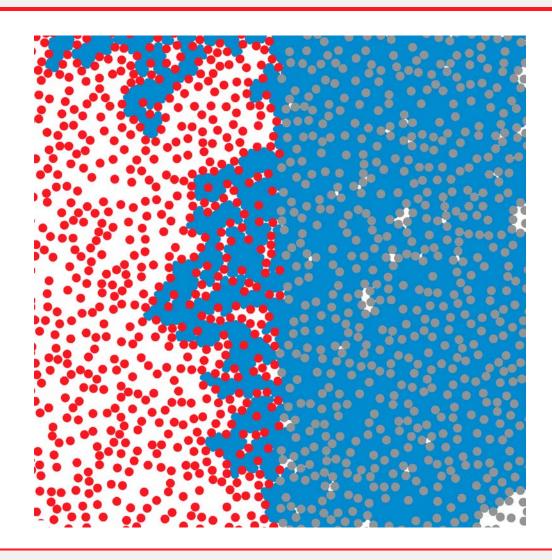
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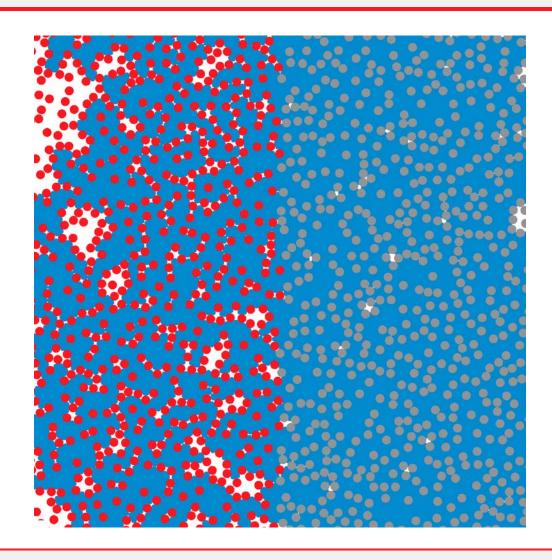
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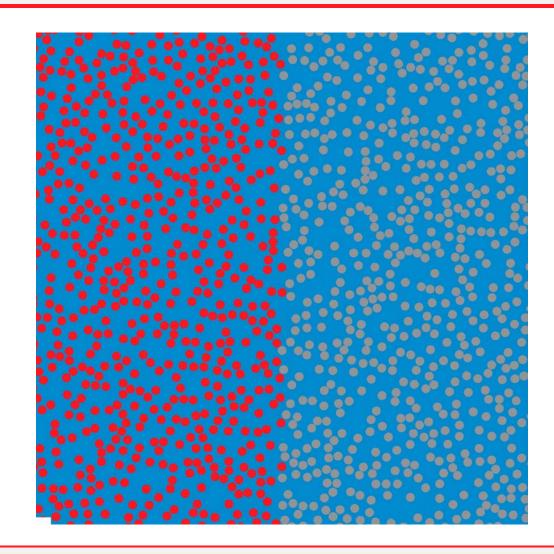


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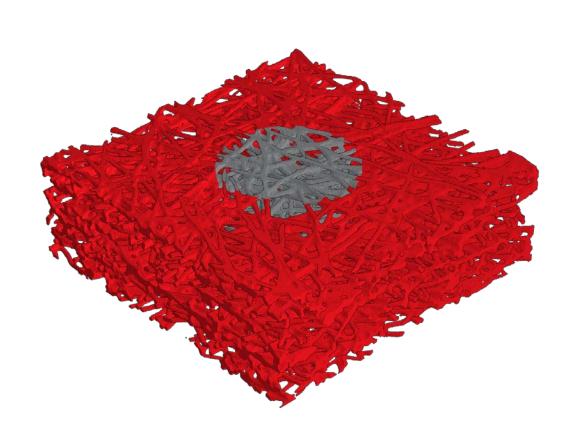
- Contact angle 0°
- Contact angle 40°
- Water (non-wetting)
- Air (wetting)





### **Structure with Variable Wettability**

Marked a cylinder as area with higher wettability





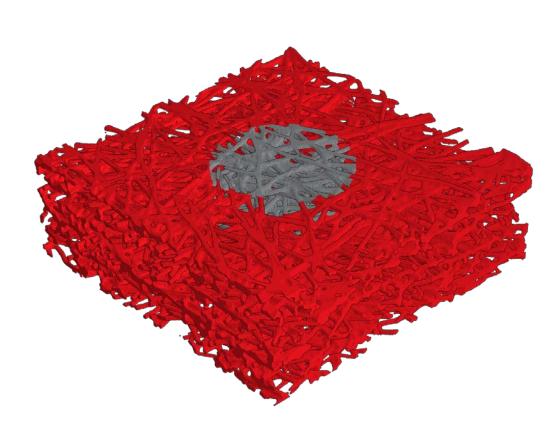
#### **Structure with Variable Wettability**

Marked a cylinder as area with higher wettability

#### Other options:

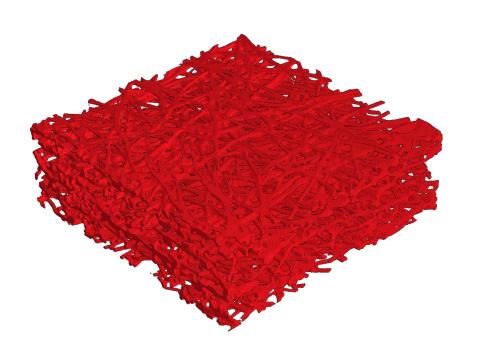
- distinguish between binder and fibers
- mark individual fibers

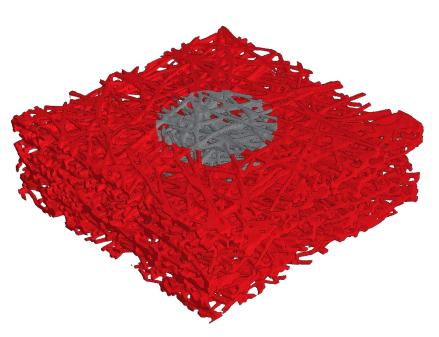
**..**,





#### **GDL Models**





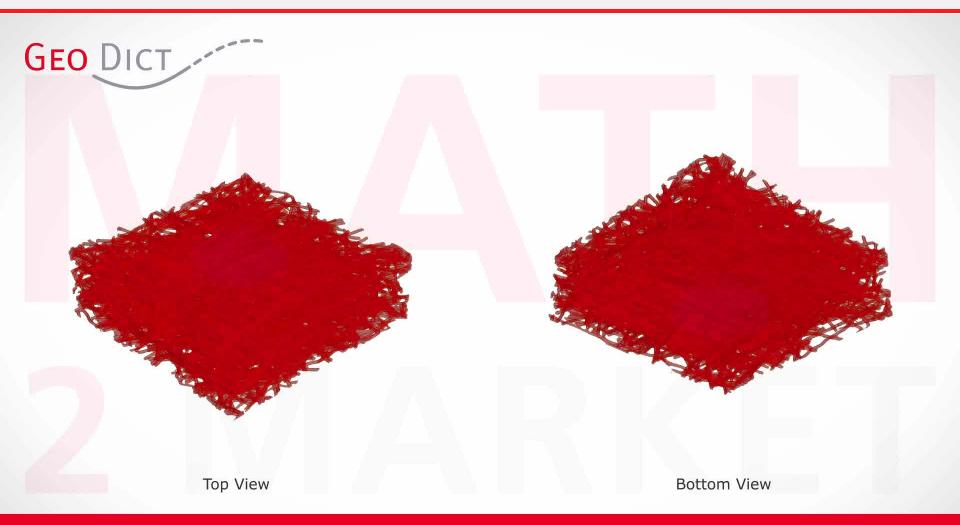
Constant Contact Angle

Two Different Contact Angles





# Water Entering into the GDL

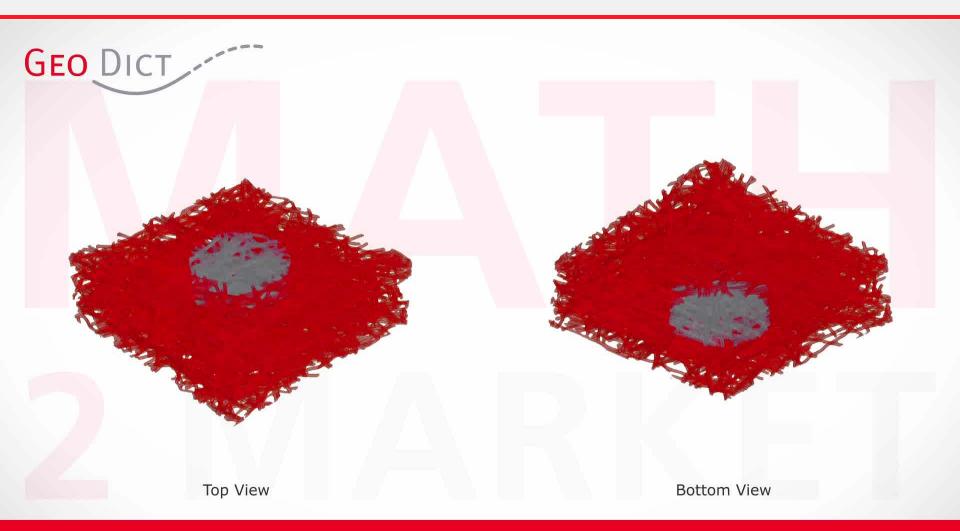


SatuDict Simulation with constant contact angle; uncompressed





# Water Entering into the GDL

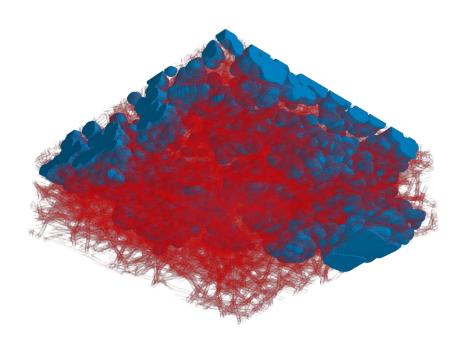


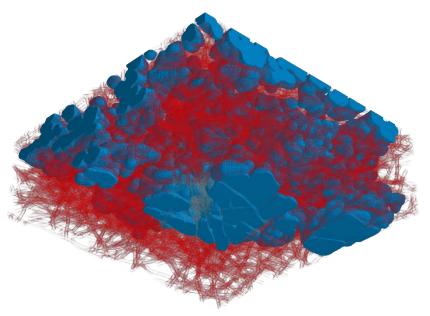
SatuDict Simulation with two different contact angles; uncompressed





# Comparison





**Constant Contact Angle** 

Two Different Contact Angles



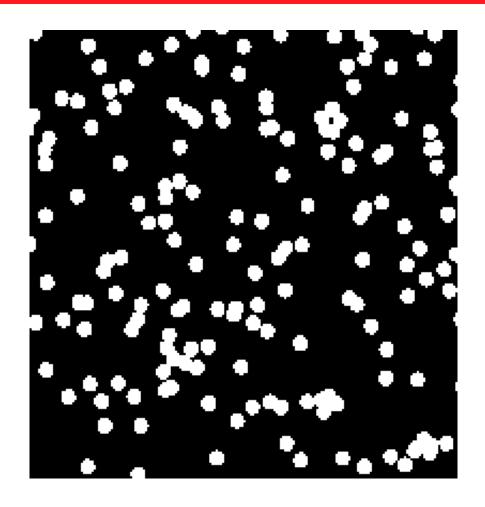


# **Relative Permeability**





# **Saturation Dependent Permeability**



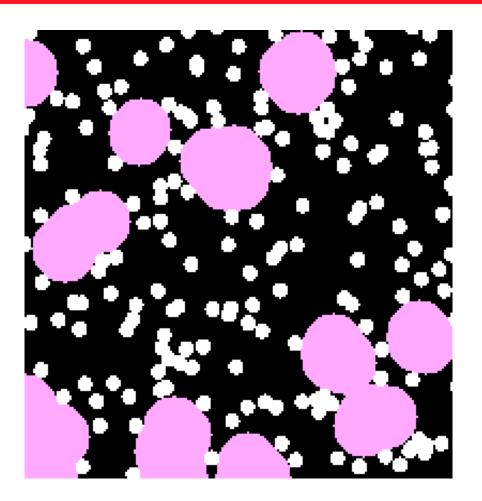




# **Saturation Dependent Permeability**

For each saturation:

1. Determine phase distribution

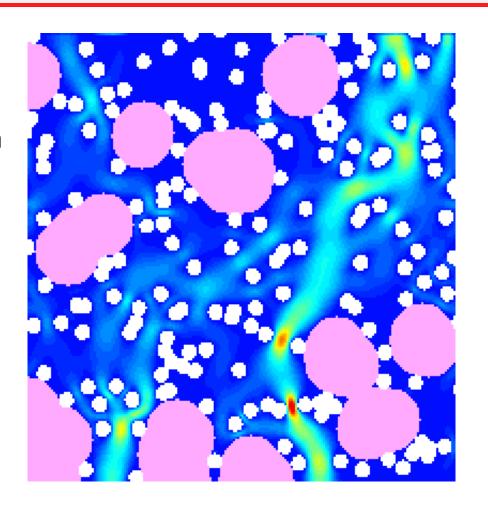




### **Saturation Dependent Permeability**

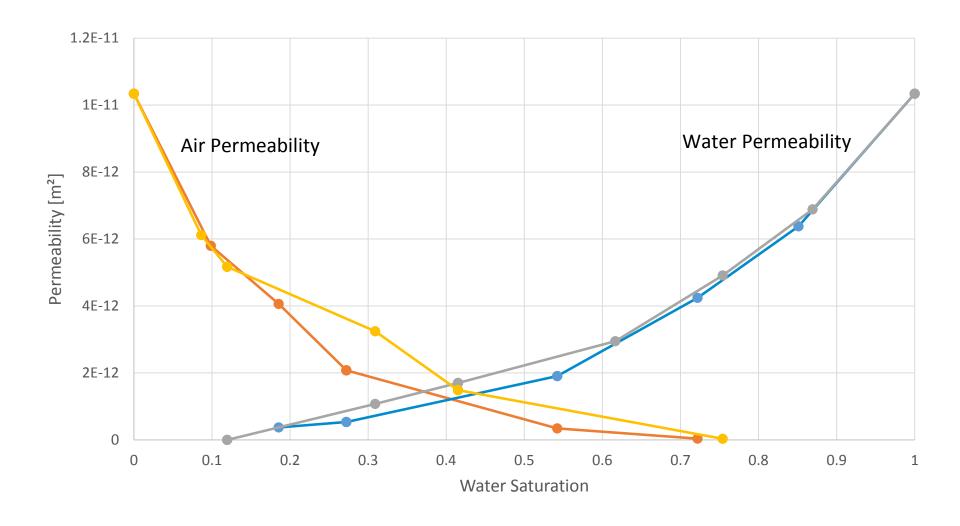
### For each saturation:

- 1. Determine phase distribution
- 2. Calculate single-phase flow (solve Stokes equation)
- Find permeability
  (average flow velocity)





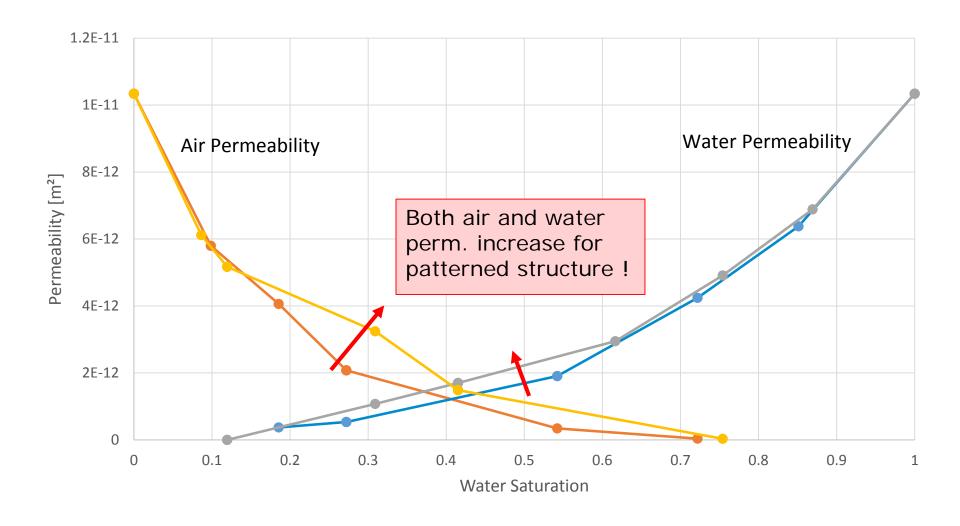
### **Through-Plane Permeability (Uncompressed GDL)**







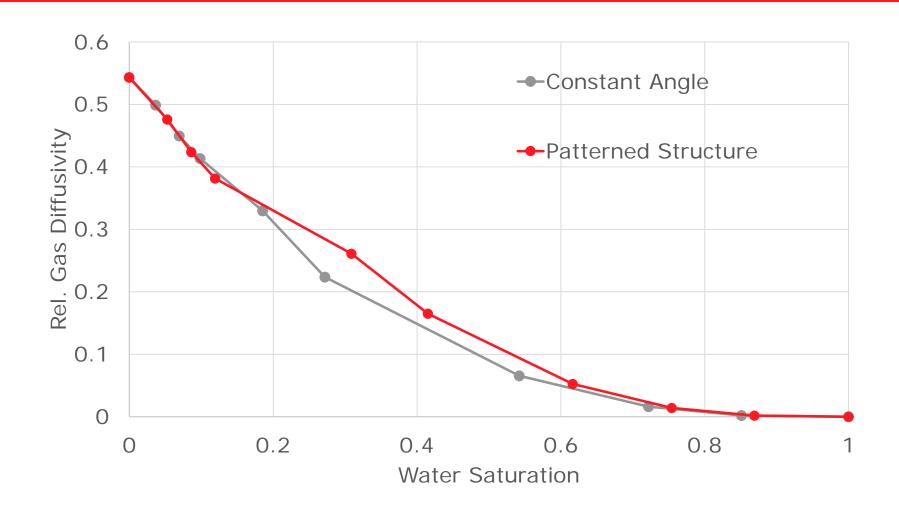
### Through-Plane Permeability (Uncompressed GDL)







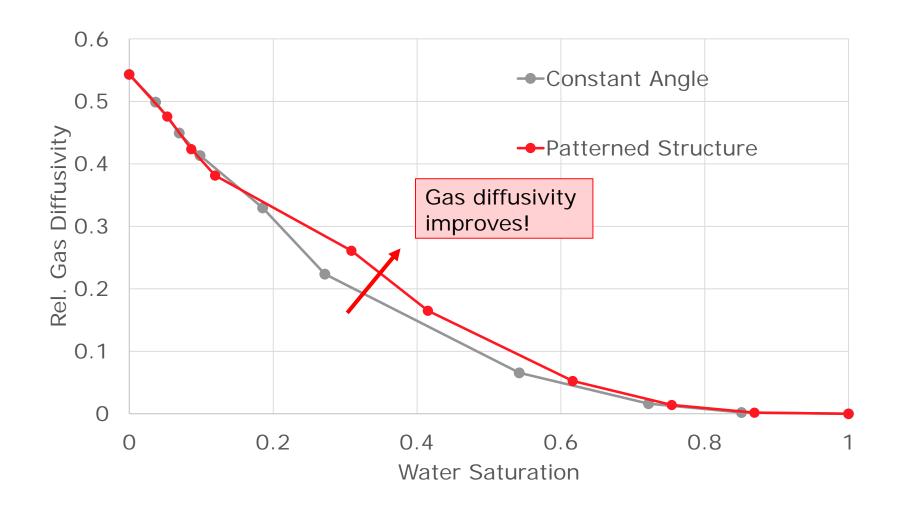
### **Through-Plane Diffusivity (Uncompressed GDL)**







### **Through-Plane Diffusivity (Uncompressed GDL)**







### **Relative Permeability – Computational Costs**

### Challenge:

- Parameter that is most expensive to compute:
  - Requires to solve one flow problem per saturation level

#### Observation:

Low saturation states are computationally most expensive



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#### Improvements:

- Restart of computations
  - Compute permeability from highest to lowest saturation state
  - Use result from previous computation to speed up the next one



### **Relative Permeability - Computational Costs**

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#### Observation:

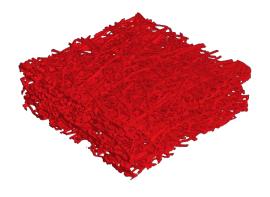
Low saturation states are computationally most expensive

#### Improvements:

- Restart of computations
  - Compute permeability from highest to lowest saturation state
  - Use result from previous computation to speed up the next one
- New stopping criterion:
  - Relative error compared to the permeability of the fully saturated state



### Speed-Up



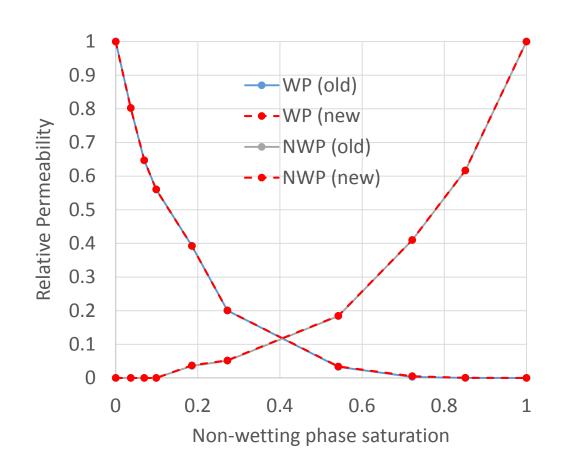
### Comparison:

- Uncompressed GDL
- 600 x 600 x 200 Voxels
- 10 Saturation levels each
- Parallelization: 12x

#### Runtime needed:

Old: 6h 22 min

New: 58 min





### **Summary**

- 1. Generated a 3D GDL model
- Computed compressed structure
- Computed permeability
- 4. Computed water saturation with different contact angles
- 5. Computed transport properties for different water saturations
- 6. Speed-up of permeability computations

# Thank You!

#### Thanks to:

- Steffen Schwichow (Math2Market)
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- Funding through OptiGaall project

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